



ISSCC 2017

SESSION 17
TX and RX
Building Blocks

Rapid and Energy-Efficient Molecular Sensing Using Dual mm-Wave Combs in 65nm CMOS:

A 220-to-320GHz Spectrometer with 5.2mW Radiated Power and 14.6-to-19.5dB Noise Figure

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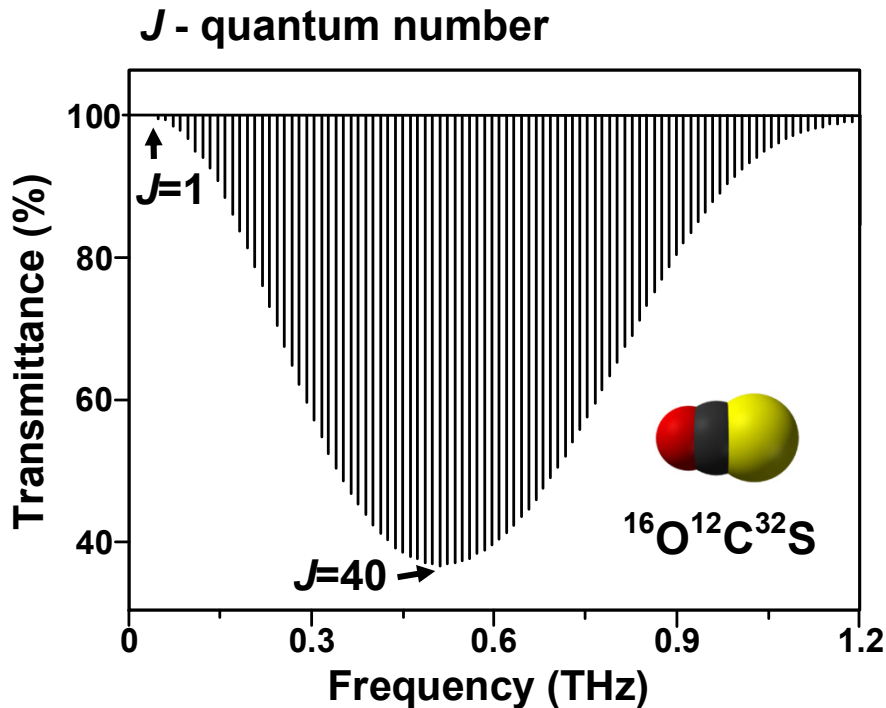


Massachusetts
Institute of
Technology

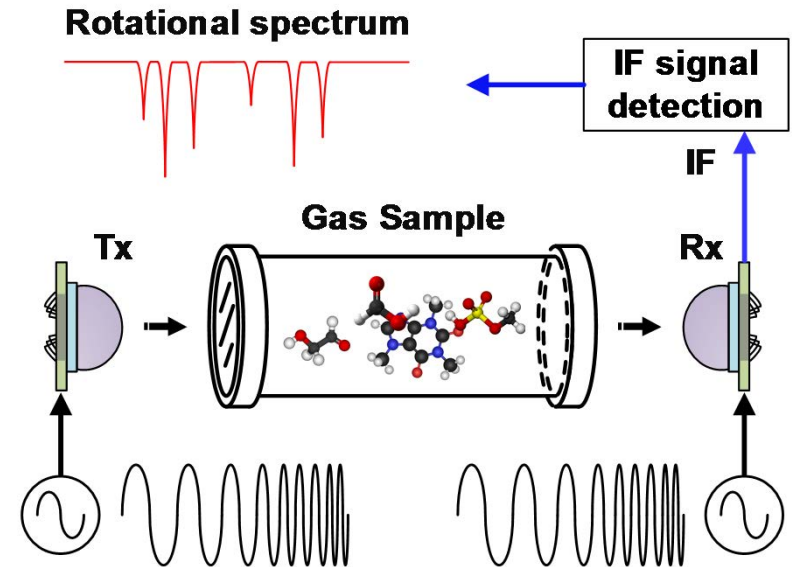
Outline

- **Background**
- **Dual-Frequency-Comb Spectroscopy**
- **Architecture and Circuit Design**
- **Measurement Results**
- **Conclusions**

mm-Wave/THz Rotational Spectroscopy



Peak absorption intensity at mmW/sub-THz band

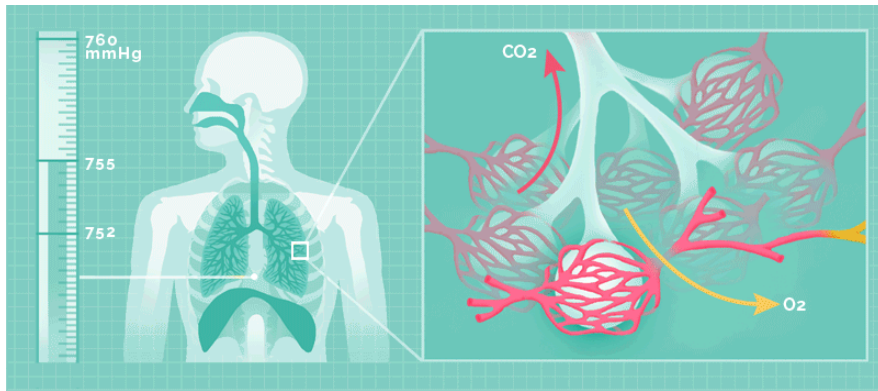


Detection of rotational spectral lines using EM wave

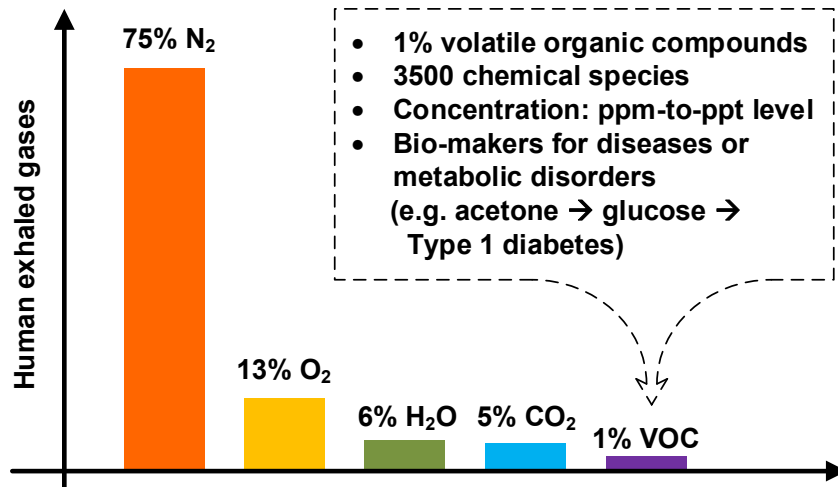
- **Rotation of polar molecules leads to absorption spectrum**
 - Maximum absorption in mmW/lower-THz range
 - Sub-MHz Doppler-limited linewidth \rightarrow high selectivity

Portable Molecular Sensor: Applications

- Human breath analyzer for biomedical diagnosis



[tabletopwhale.com]



- Environment monitoring for toxic gas leakage

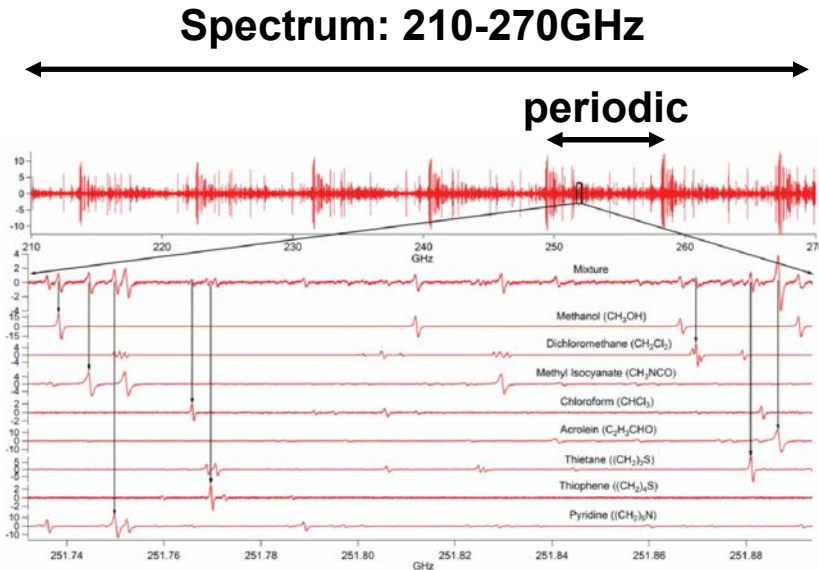
- Sensor network
- UAV platform



[www.dji.com]



Challenges of Chip-Scale Spectrometer



[C. F. Neese, IEEE Sensors Journal, 2012]

Molecule	Frequency (GHz)	Toxic?	Flammable ?
Carbon Monoxide (CO)	230.538001	Y	Y
Sulfur Dioxide (SO ₂)	251.199668		
Hydrogen Cyanide (HCN)	265.886441		Y
Hydrogen Sulfide (H ₂ S)	300.511959		Y
Nitric Oxide (NO)	250.436966	Y	
Nitrogen Dioxide (NO ₂)	292.987169	Y	
Nitric Acid (HNO ₃)	256.657731	Y	
Ammonia (NH ₃)	208.145904	Y	
Carbonyl Sulfide (OCS)	231.060989	Y	Y
Ethylene Oxide (C ₂ H ₄ O)	263.292515	Y	
Acrolein (C ₃ H ₄ O)	267.279359	Y	
Methyl Mercaptan (CH ₃ SH)	227.564672	Y	
Methyl Isocyanate (CH ₃ NCO)	269.788609	Y	
Methyl Chloride (CH ₃ Cl)	239.187523	Y	Y
Methanol (CH ₃ OH)	250.507156	Y	Y
Acetone (CH ₃ COCH ₃)	259.6184	Y	Y
Acrylonitrile (C ₂ H ₃ CN)	265.935603	Y	Y

[Source: HITRAN.org]

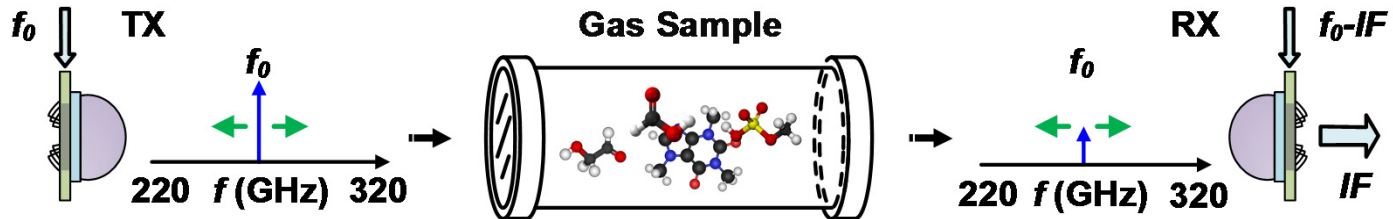
- **High selectivity**
 - Wideband(100GHz), high resolution(10kHz) spectrometer
- **High sensitivity, fast scanning**
 - High radiated power (below saturation), low noise detection
- **High energy efficiency**

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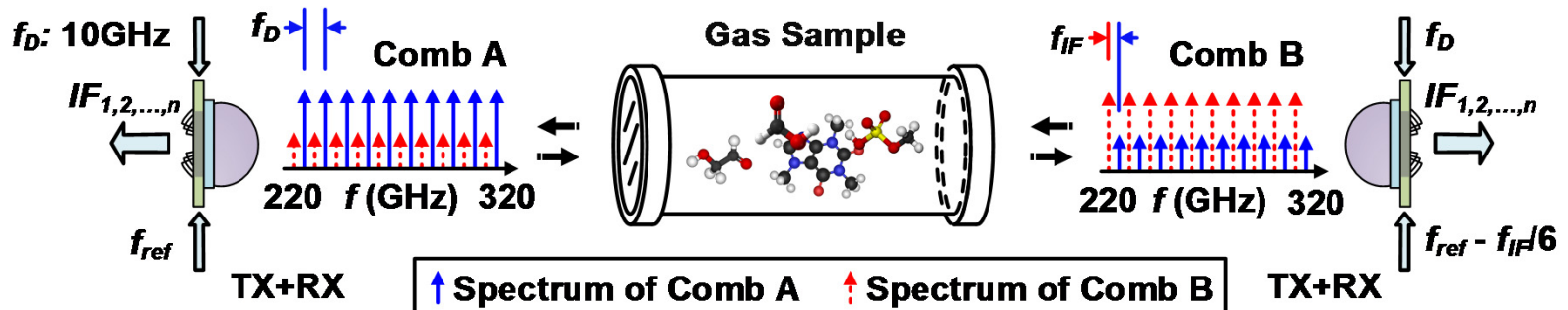
Dual-Frequency-Comb Spectroscopy

Conventional single-tone spectroscopy



- Single frequency sweep (e.g. ~3 hours for 100GHz bandwidth, $\tau_{int}=1\text{ms}$)

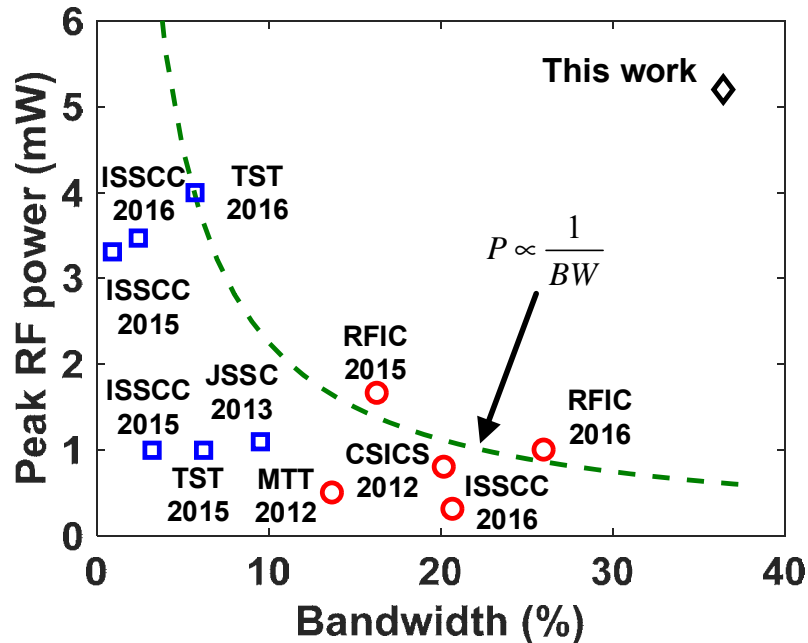
Dual-frequency-comb spectroscopy



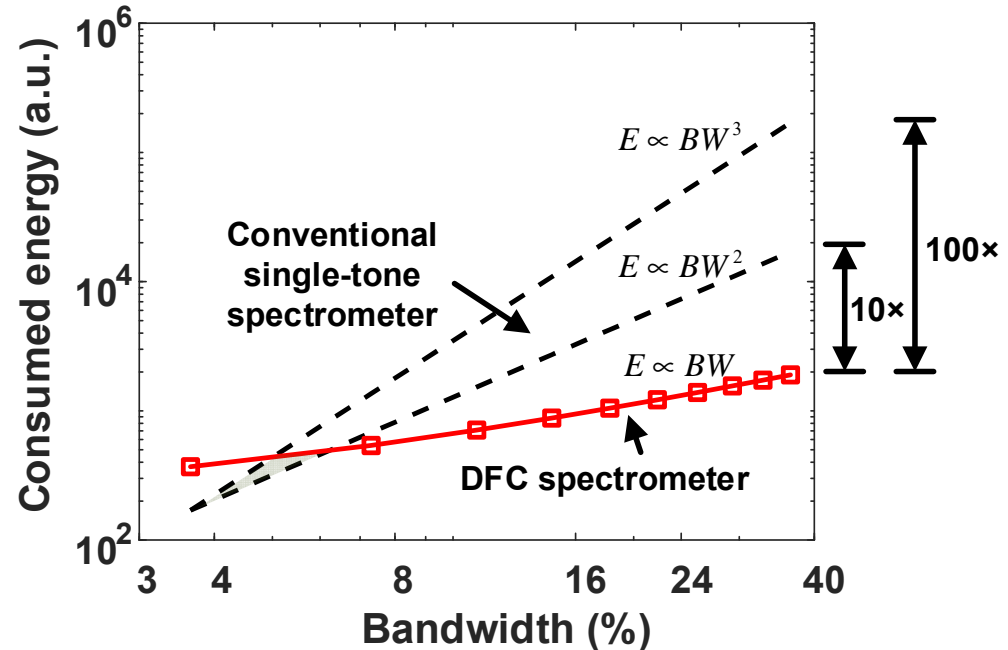
- Simultaneous scanning using 20 comb lines (8 minutes for 100GHz bandwidth, $\tau_{int}=1\text{ms}$)

Energy Efficiency Improvement

Radiated power of silicon-based sources above 200GHz



Total energy consumption for full-band scanning



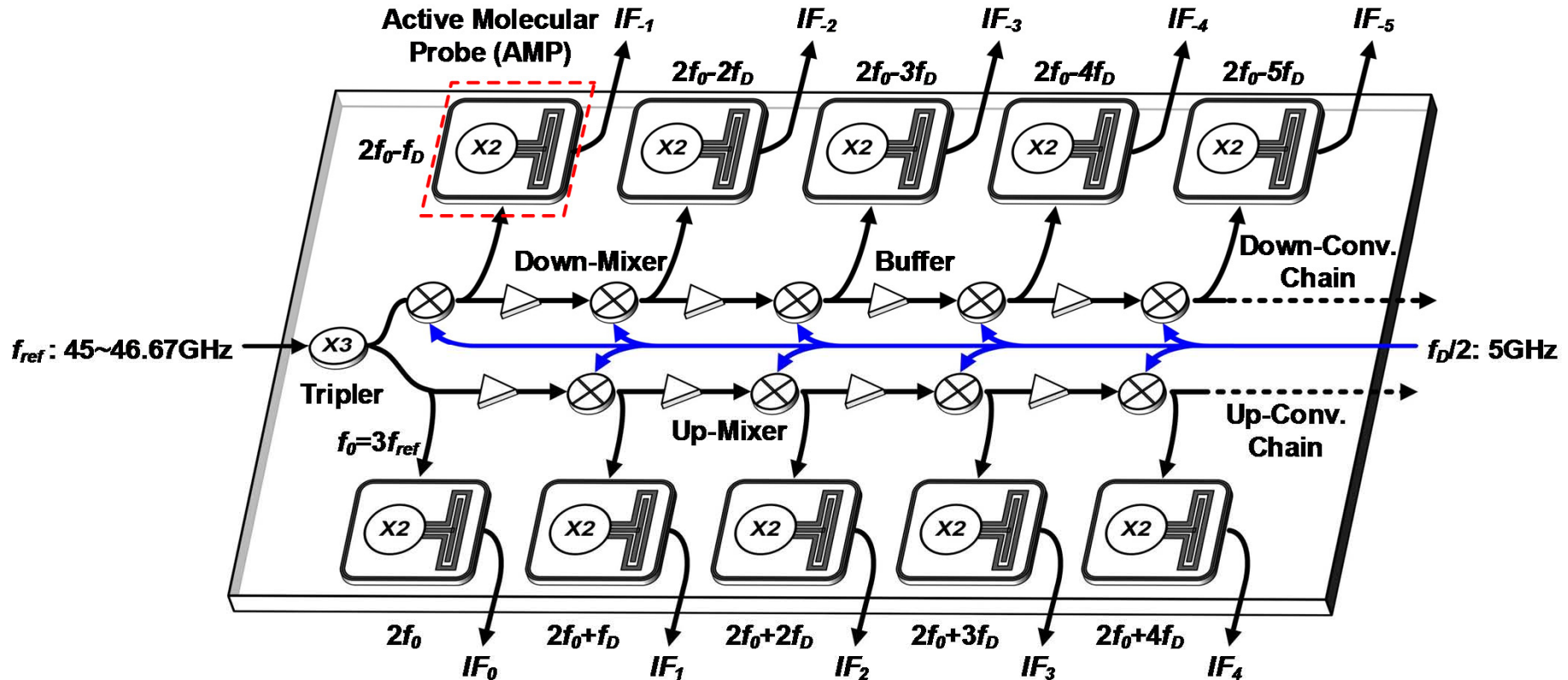
□ Radiated ○ On-wafer measured with an assumed 50% radiation efficiency

- Dual frequency combs (DFC) scheme breaks the conventional efficiency-bandwidth tradeoff using parallelism
- Linear scalability between bandwidth and energy consumption

Outline

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- Dual-Frequency-Comb Spectroscopy
- **Architecture and Circuit Design**
- Measurement Results
- Conclusions

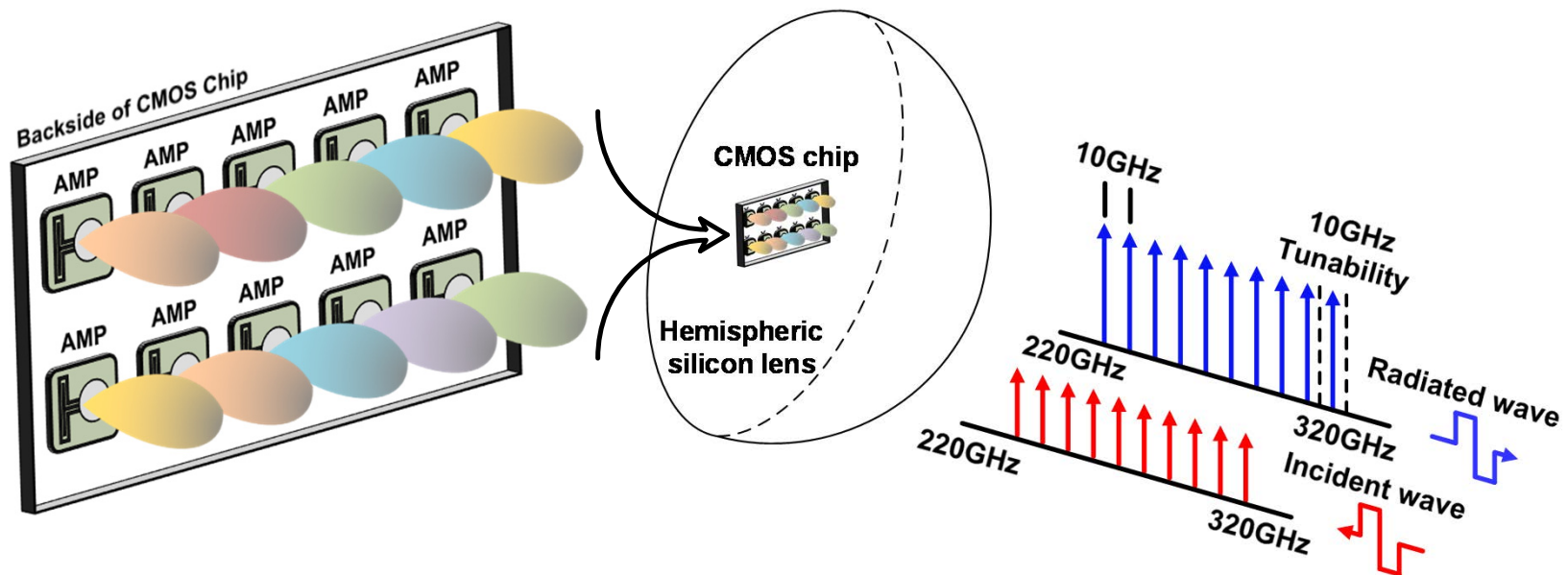
Architecture of A 220-to-320GHz Comb



- **Tunable transceiver: 10 active molecular probes (AMP)**
 - Seamless coverage of 100GHz bandwidth
 - Simultaneous transmit and receive \rightarrow $\sim 2x$ higher efficiency

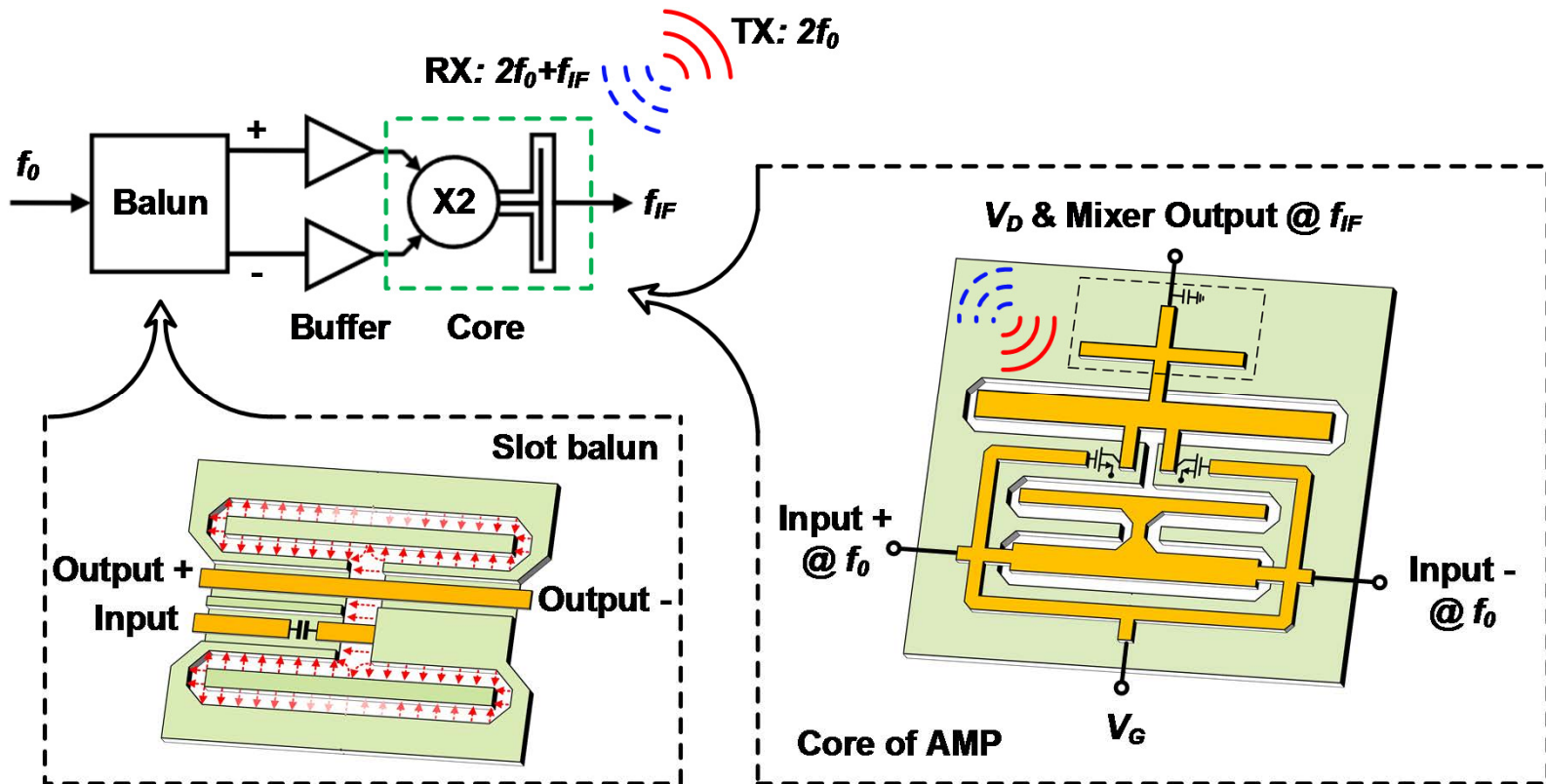
Distributed Comb-Spectral Radiation

- **On-chip backside radiation through 10 radiators**
 - Improved antenna efficiency by narrowband operation
- **High-resistivity hemispheric silicon lens is used**
 - Lower sensitivity to the radiator offset from the center (compared to hyper-hemispheric lens)
 - No additional beam collimation



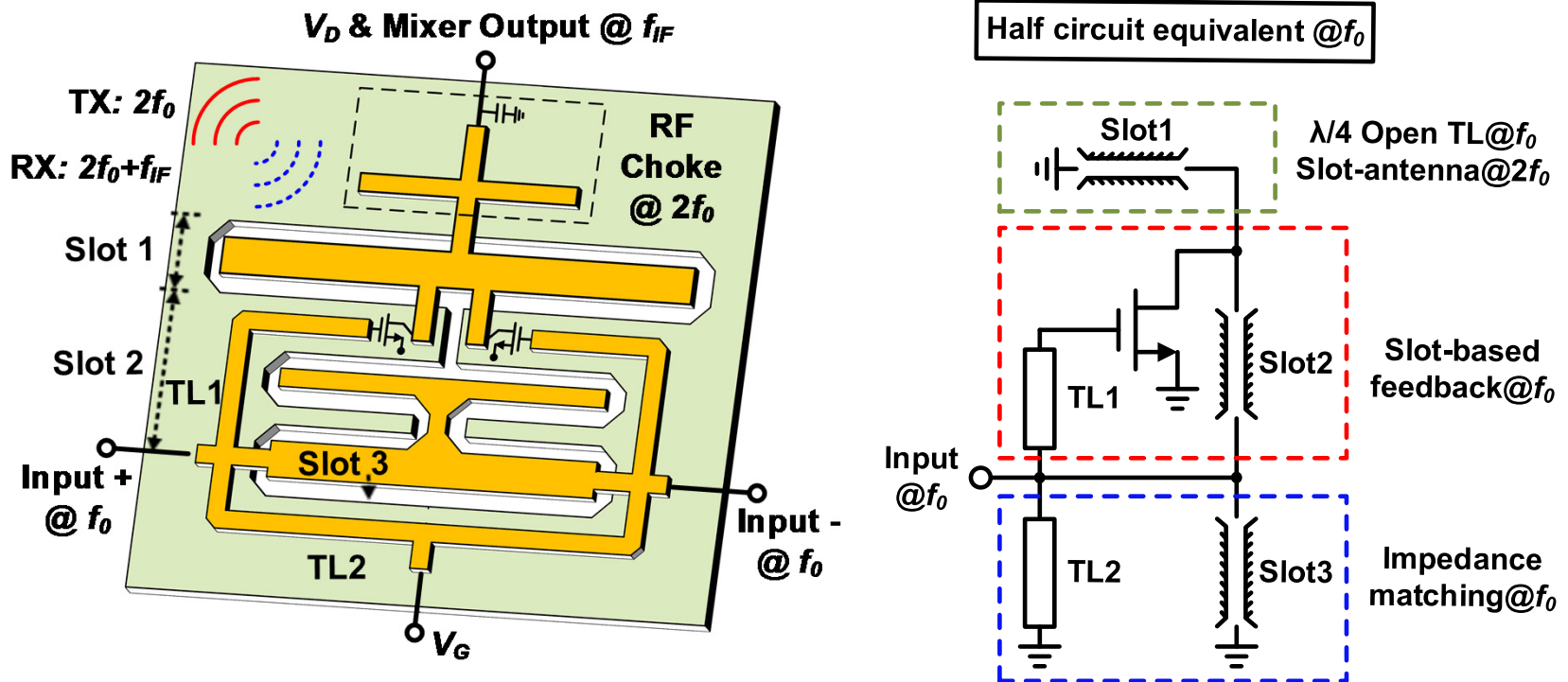
Active Molecular Probe (AMP)

- **Multi-functional module simultaneously performs**
 - Highly-efficient frequency doubling
 - Low-noise heterodyne sub-harmonic down mixing
 - Efficient antenna for input/output radiation waves



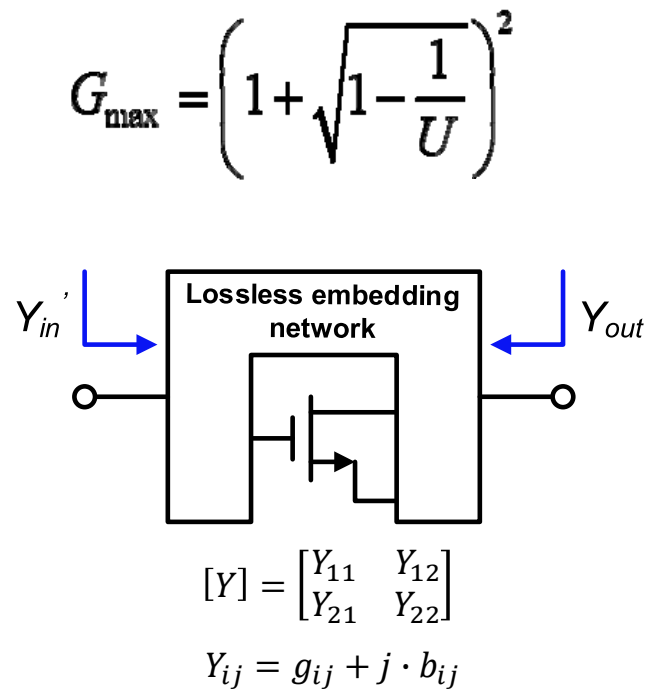
AMP TX Mode: Frequency Doubling

- **Conditions for high conversion efficiency**
 - Maximum device power gain at fundamental frequency (f_0)
 - Minimum loss at $2f_0$ (e.g. harmonic feedback to the lossy gates)
 - Instantaneous signal radiation at $2f_0$



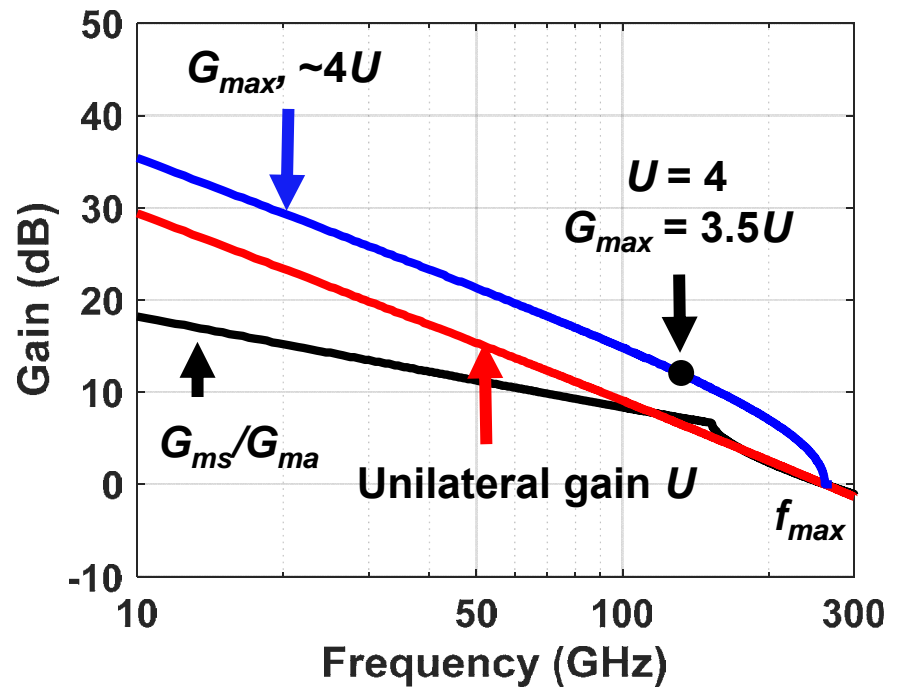
Maximum Device Power Gain G_{max}

- Upper limit of matched power gain G_{max} depends on the unilateral gain U



[R. Spence, Linear Active Networks 1968]

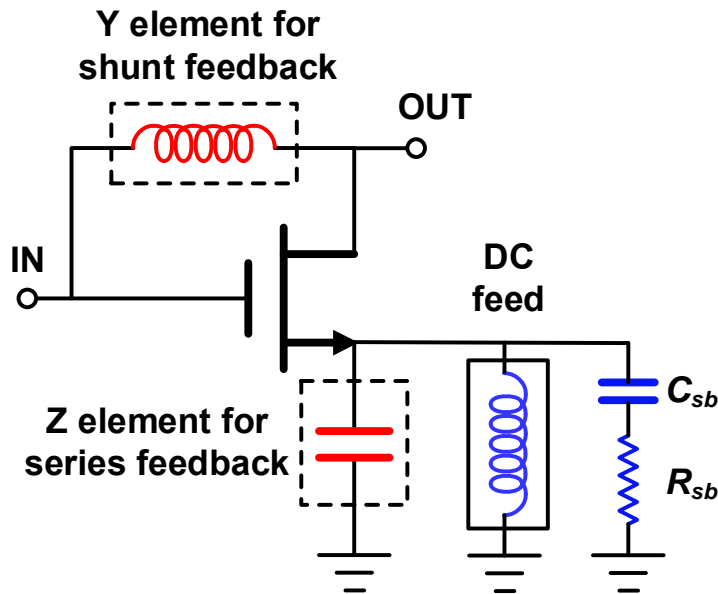
[O. Momeni, ISSCC 2013]



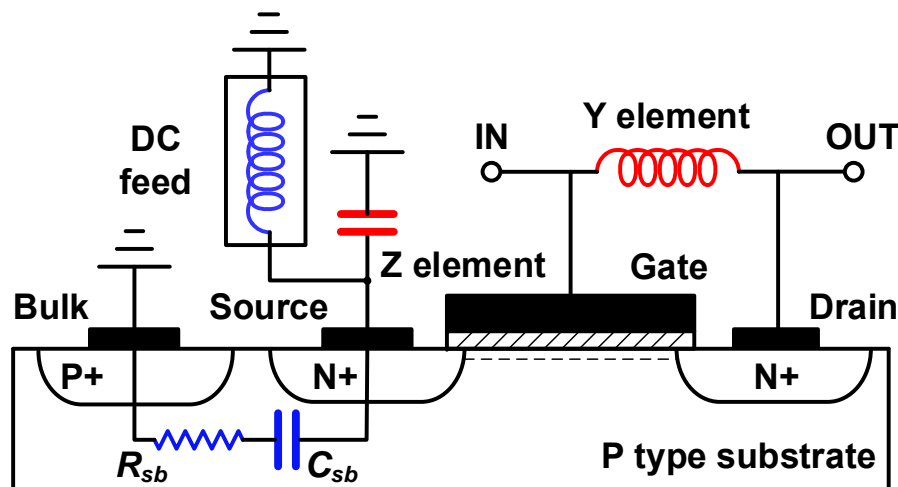
Simulation using 65nm bulk CMOS process

Conventional YZ Embedding for G_{max}

Equivalent circuit



Transistor structure

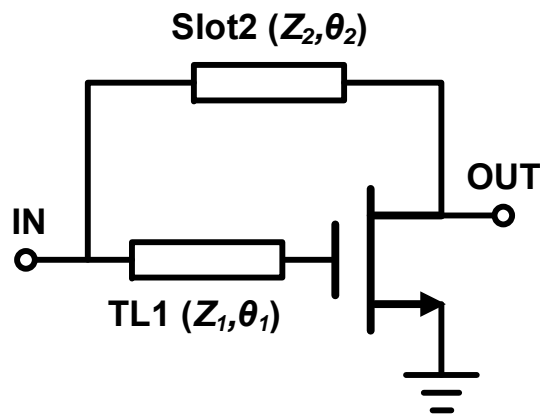


[R. Spence, Linear Active Networks 1968]

• Issues of YZ embedding with lumped elements

- Loss from DC feed to bypass source current
- Loss from parasitic resistor associated with the source
- Impractical large inductor for Y element due to distributed effect in high frequency

Dual-transmission-line (DTL) Feedback



Equations for feedback parameter calculation:

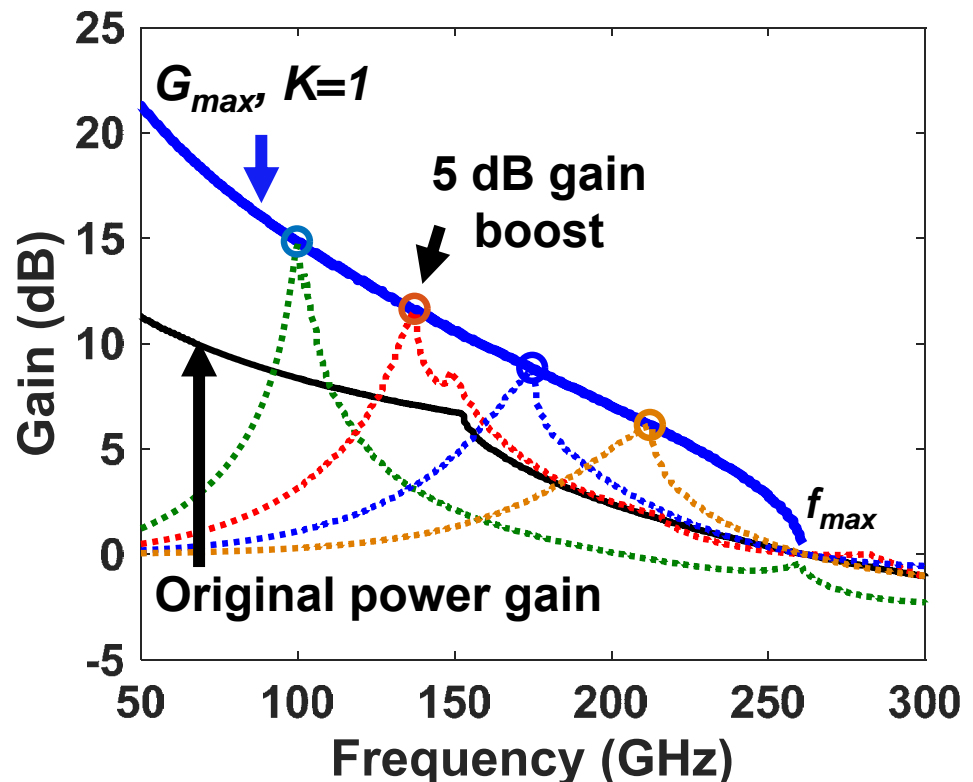
$$\begin{cases} \tan \theta_1 = \frac{1}{Z_1} \cdot \frac{1}{b_{11} - g_{11} \frac{mU b_{12} - b_{21}}{mU g_{12} - g_{21}}} \\ \sin \theta_2 = \frac{1}{Z_2} \cdot \frac{g_{11} Z_1 \sin \theta_1 (mU - 1)}{mU g_{12} - g_{21}} \end{cases}$$

where

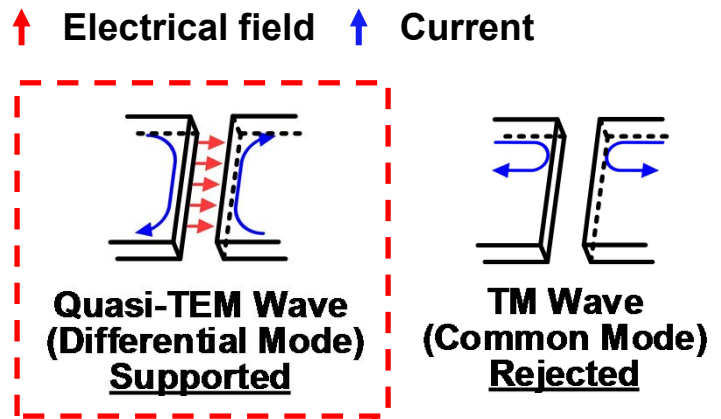
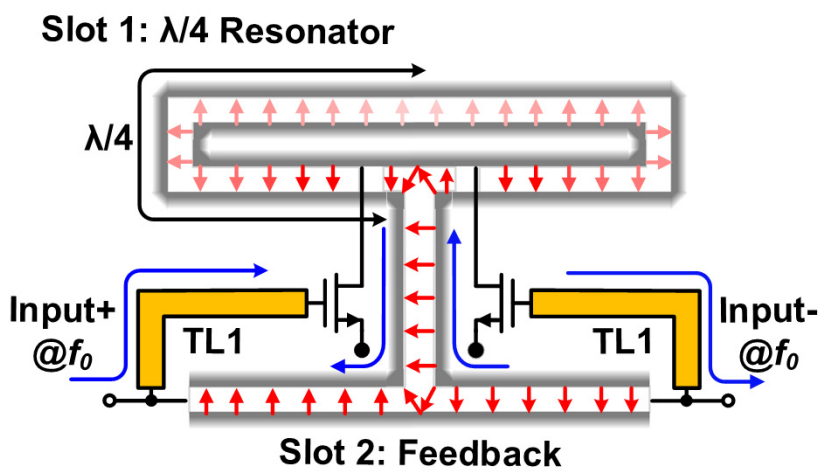
$$m = \frac{\left(1 + \sqrt{1 - \frac{1}{U}}\right) (U + \sqrt{U^2 - U} - 1)}{-\sqrt{U^2 - U}}$$

- Adopt distributed feedback elements
- Ground the source of transistor
- Achieve G_{max} accurately

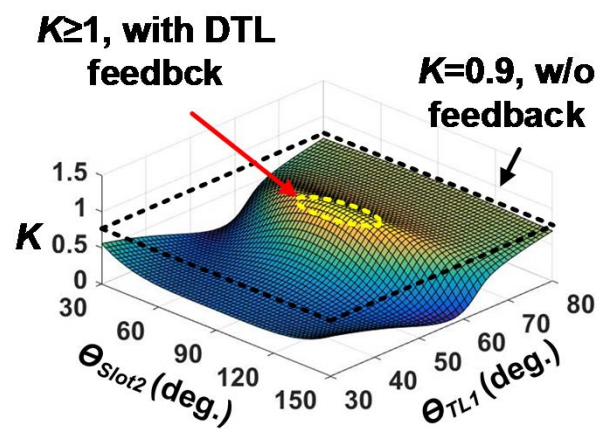
Simulation using 65nm CMOS process



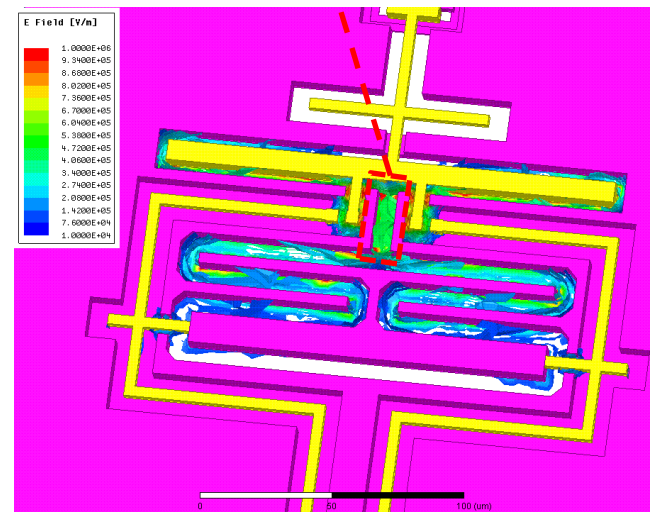
DTL Feedback Based on Slot Line @ f_0



Feedback through Slot 2



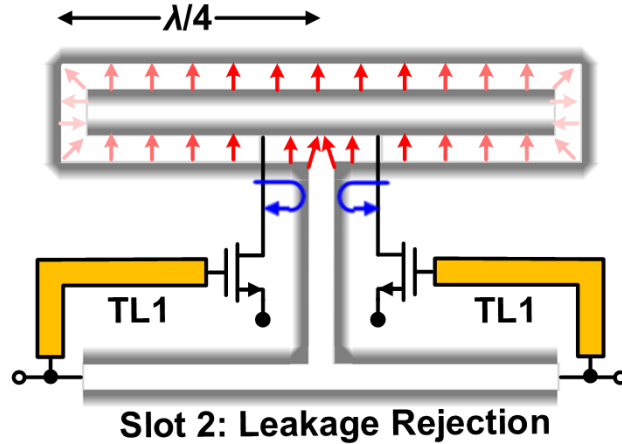
Simulated stability factor, K



E-field distribution @ f_0

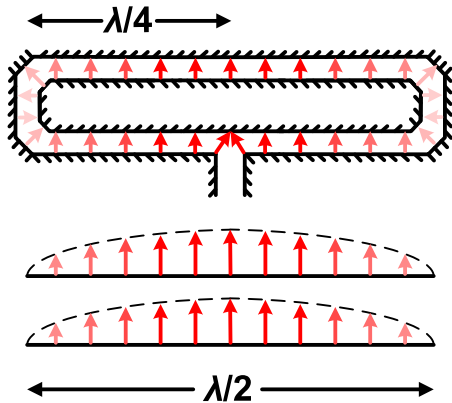
Loss Minimization and Radiation @ $2f_0$

Slot 1: Folded Slot Antenna



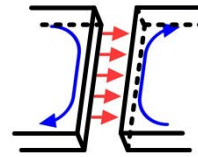
Slot 2: Leakage Rejection

Harmonic signal isolation

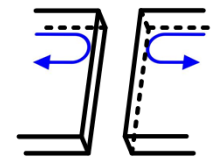


Folded-slot antenna

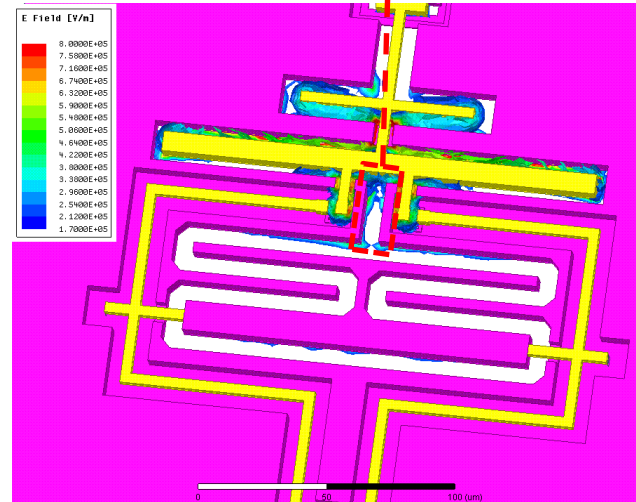
↑ Electrical field ↑ Current



Quasi-TEM Wave
(Differential Mode)
Supported

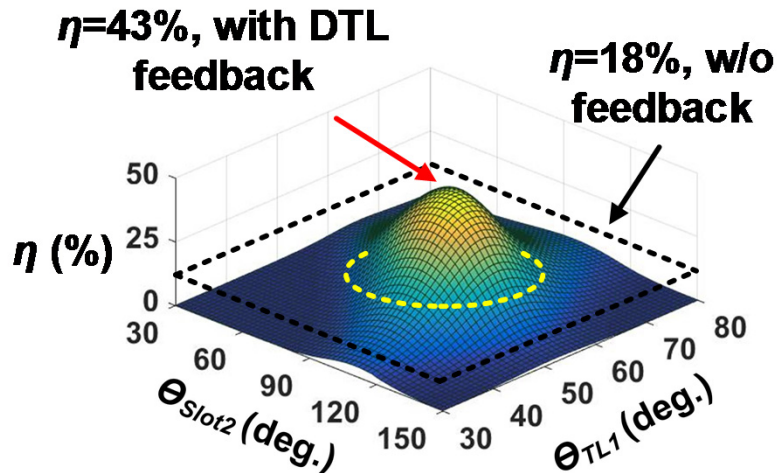


TM Wave
(Common Mode)
Rejected

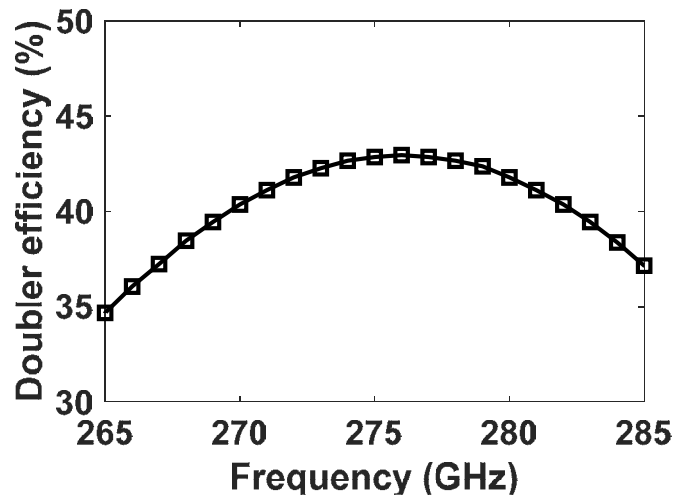


E-field distribution @ $2f_0$

Simulation Results for Doubler at 275GHz

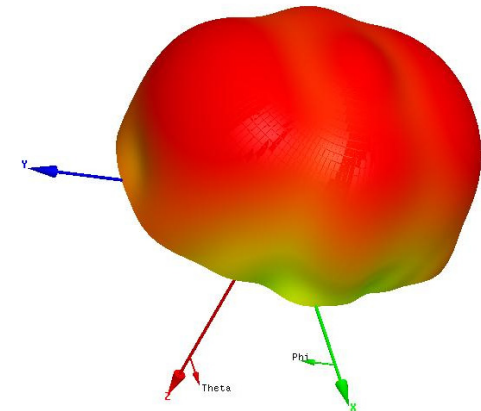
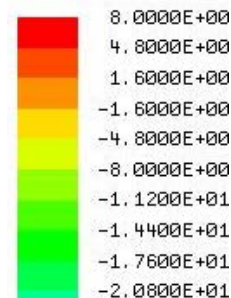


- 65nm bulk CMOS
- NMOS W/L=24 μ m/60nm
- Output power: 1.6mW
- Doubler efficiency: 43%
- Antenna efficiency: 45%



Doubler efficiency η (%)

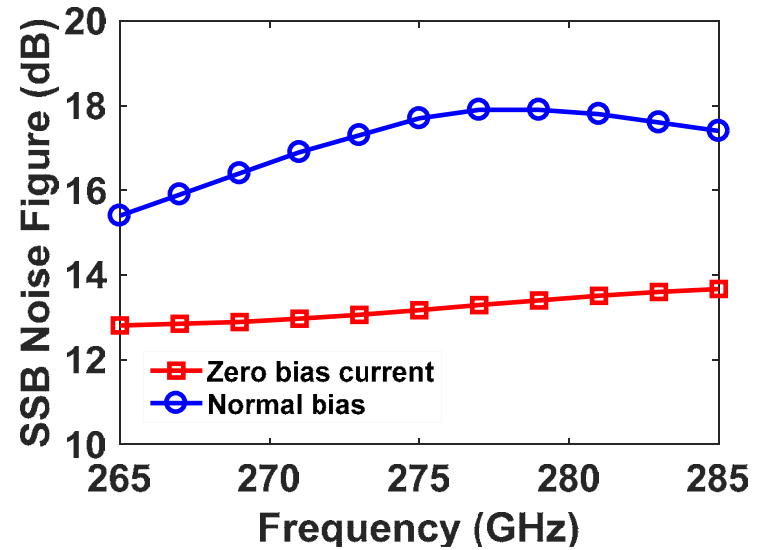
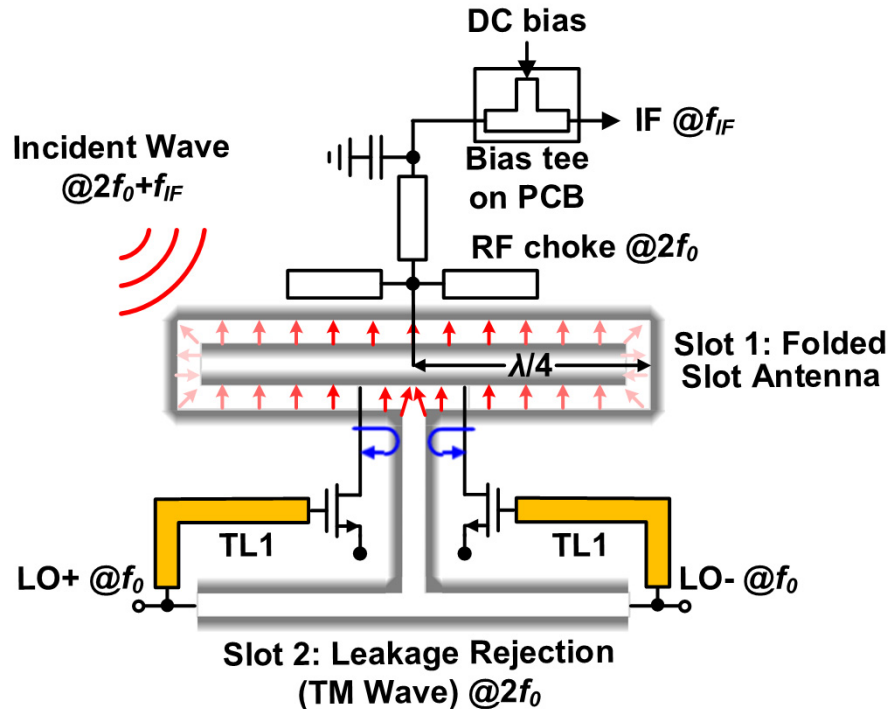
dB(DirTotal)



Antenna directivity

AMP RX Mode: Heterodyne Mixing

↑ Electrical field ↑ Current

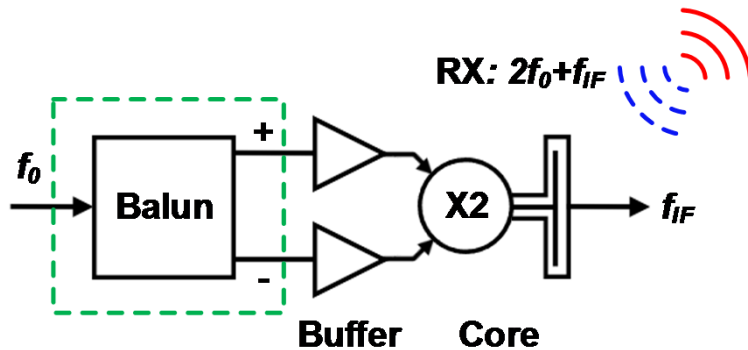


Simulated SSB noise figure

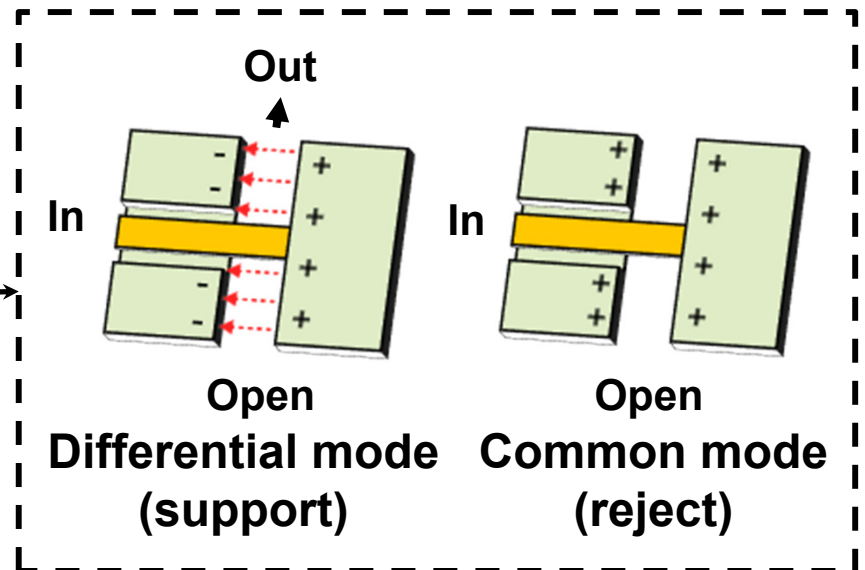
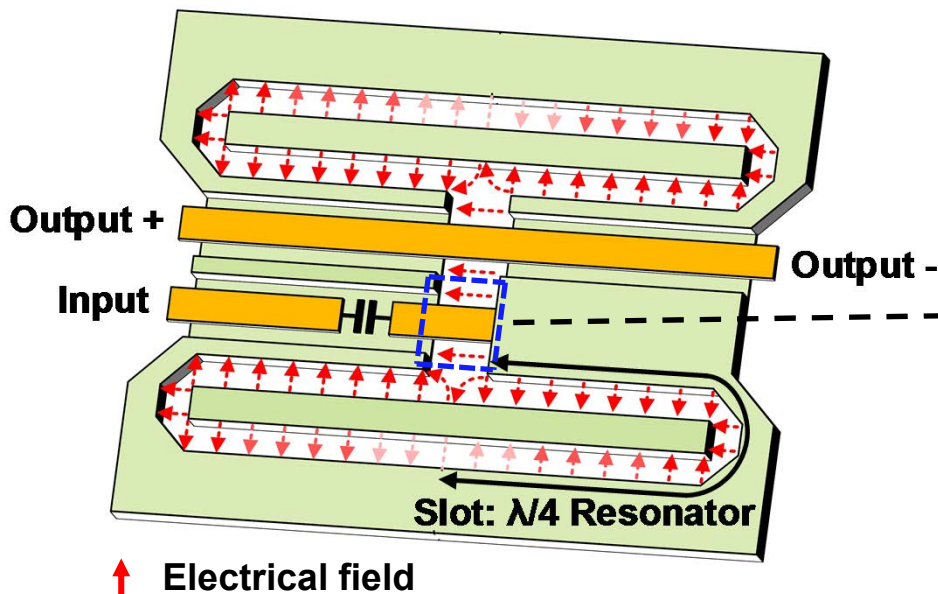
- Mixer LO signal is the same as the doubler input signal @ f_0
- Further noise reduction: zero drain bias current
→ varistor mode mixing with reduced channel noise

Slot Balun with Orthogonal Mode Filtering

Active Molecular Probe (AMP)

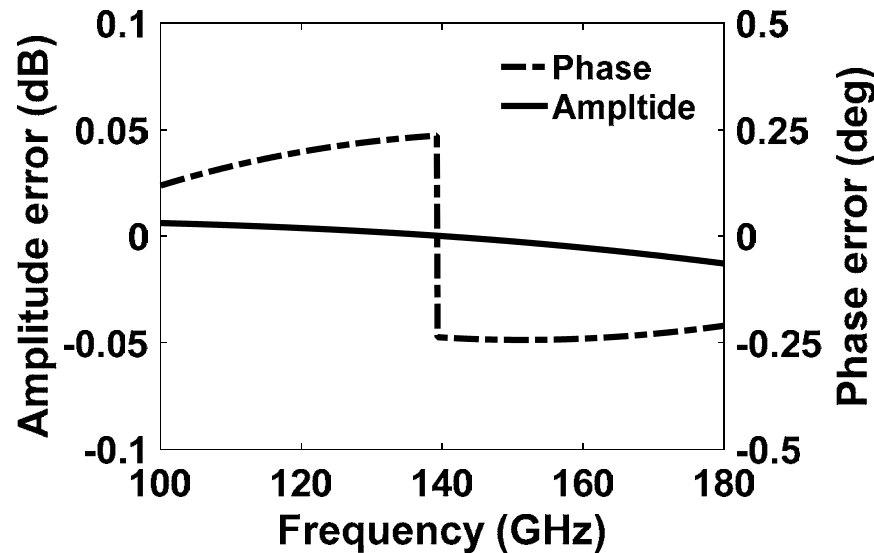


- Amplitude and phase imbalance in conventional baluns causes
 - Lower doubler efficiency
 - Higher LO signal radiation at f_0
- Proposed slot balun
 - Orthogonal mode filtering
 - Symmetric output coupling

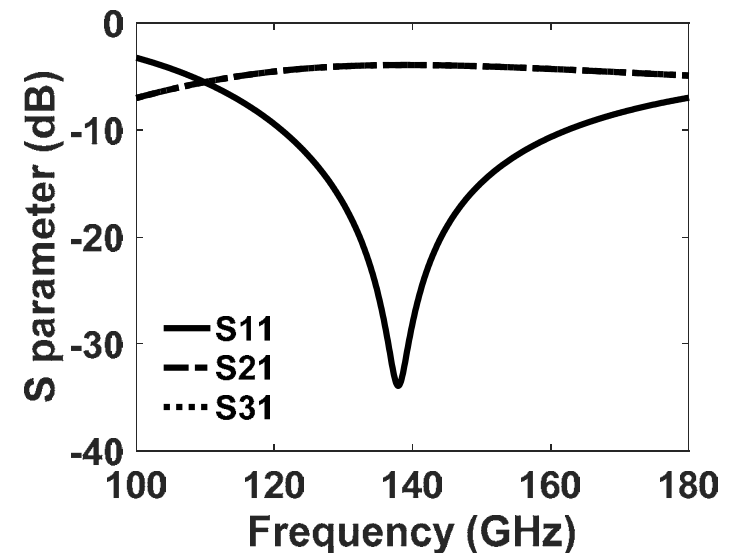


Slot Balun with Orthogonal Mode Filtering

Simulated amp. and phase error

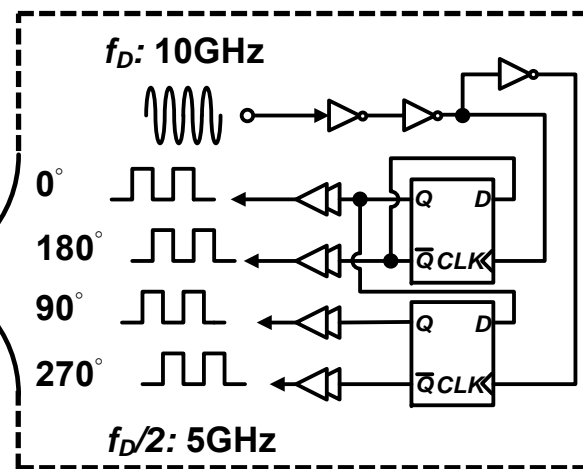
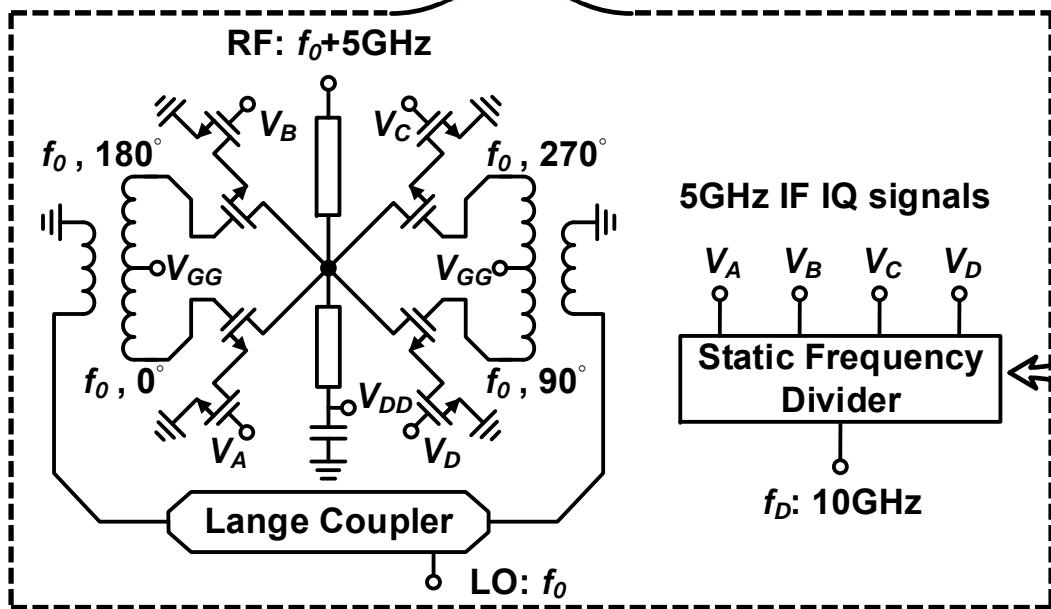
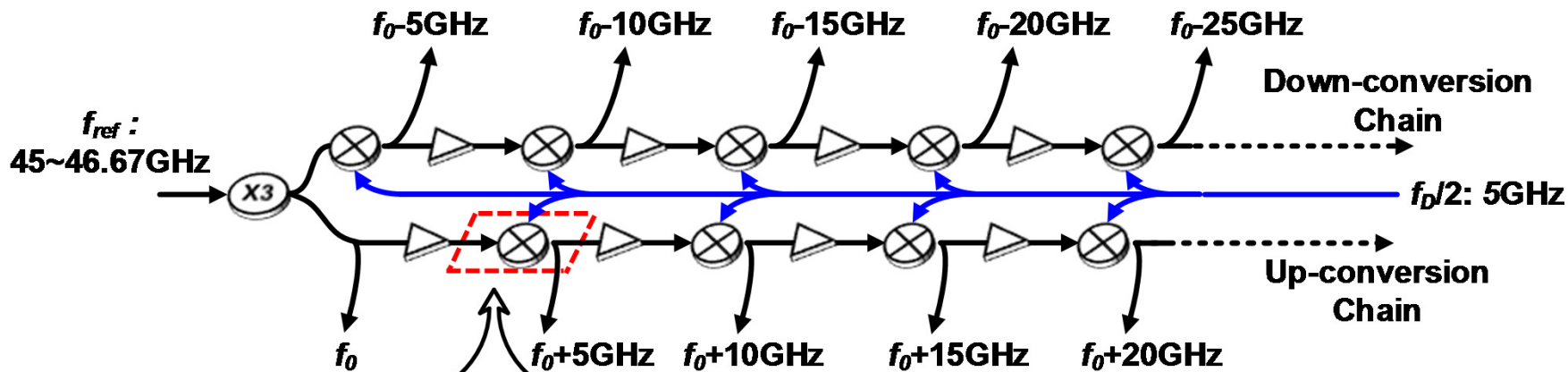


Simulated S-parameter



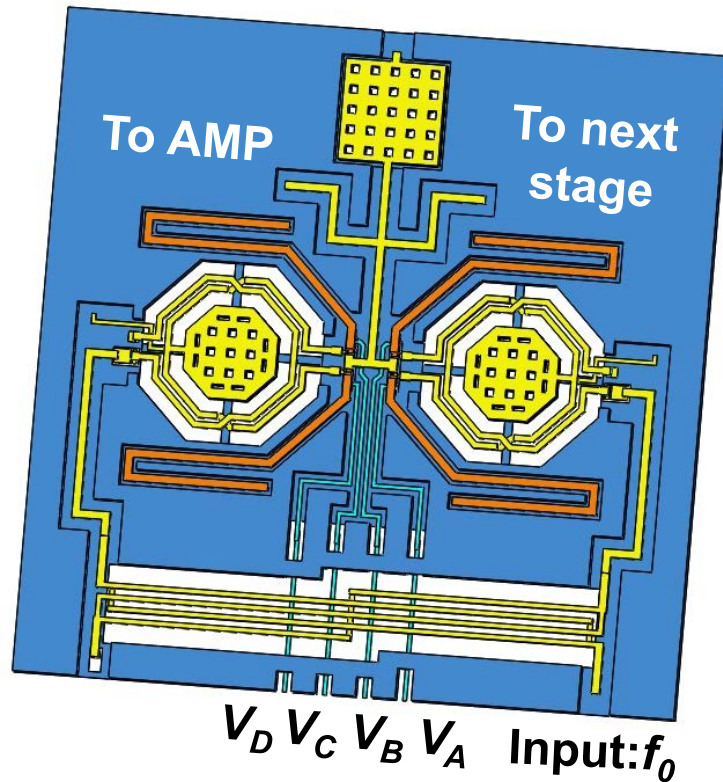
- **Nearly perfect single-ended signal to differential signal conversion without errors**
- **Minimum insertion loss: 0.9 dB**
- **-10dB return loss bandwidth: 30%**

Up/Down-Conversion Mixer



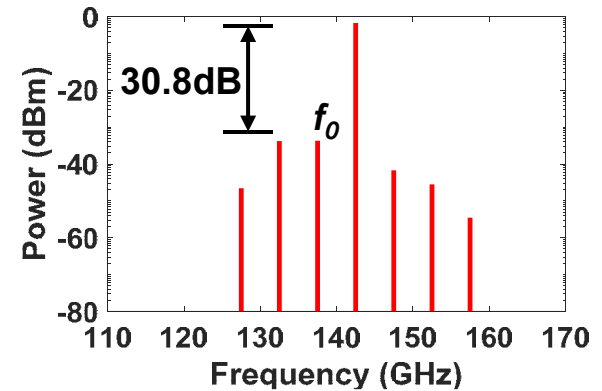
- SSB mixers configured for up/down conversion chains

Up/Down-Conversion Mixer

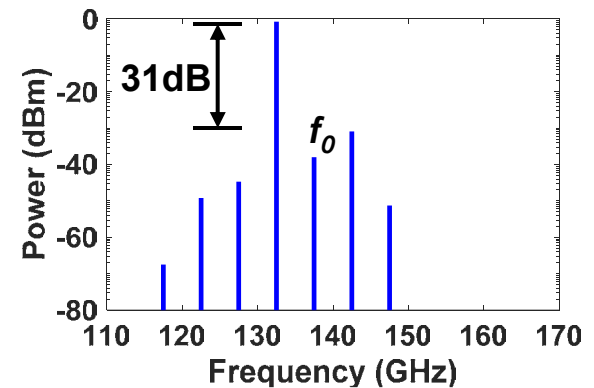


$$\text{Phase}(V_A, V_B, V_C, V_D) = (0^\circ, 180^\circ, 90^\circ, 270^\circ)$$

$$\text{Phase}(V_A, V_B, V_C, V_D) = (0^\circ, 180^\circ, 270^\circ, 90^\circ)$$



Up sideband conv.



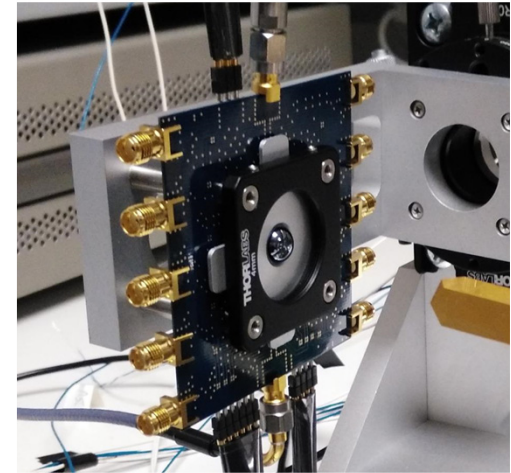
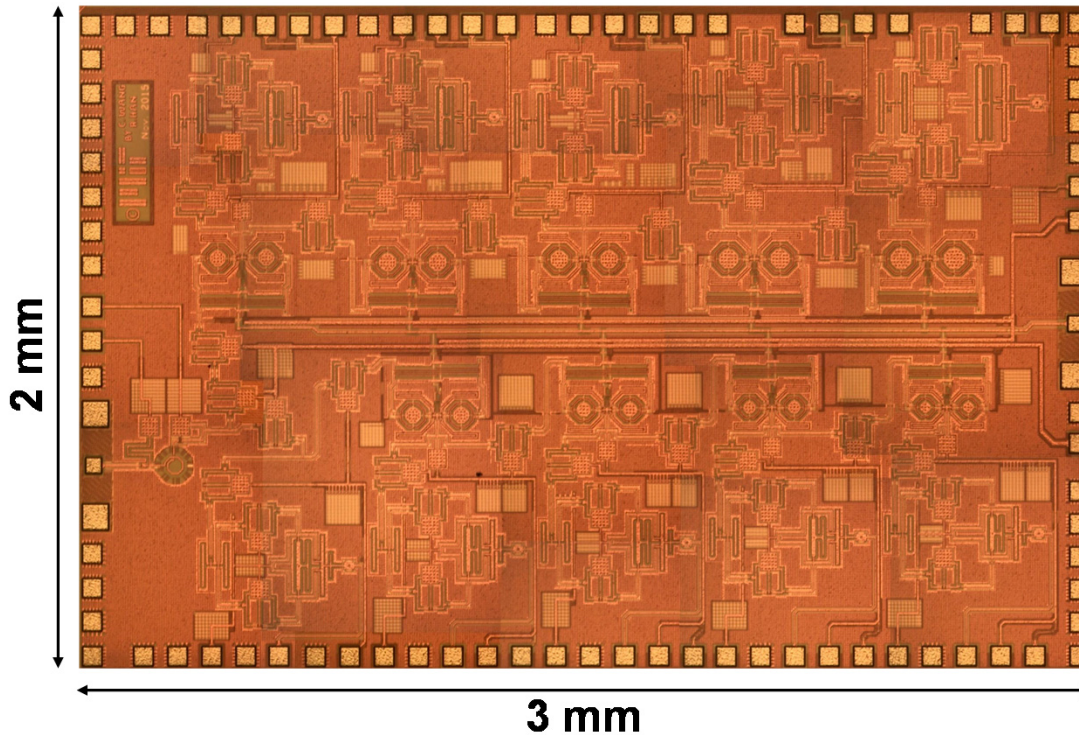
Down sideband conv.

- IF phase configuration \rightarrow up or down sideband selection
- Low conversion loss: 2.3 dB
- Rejection of image, LO and inter-modulation signals: $>30\text{dB}$

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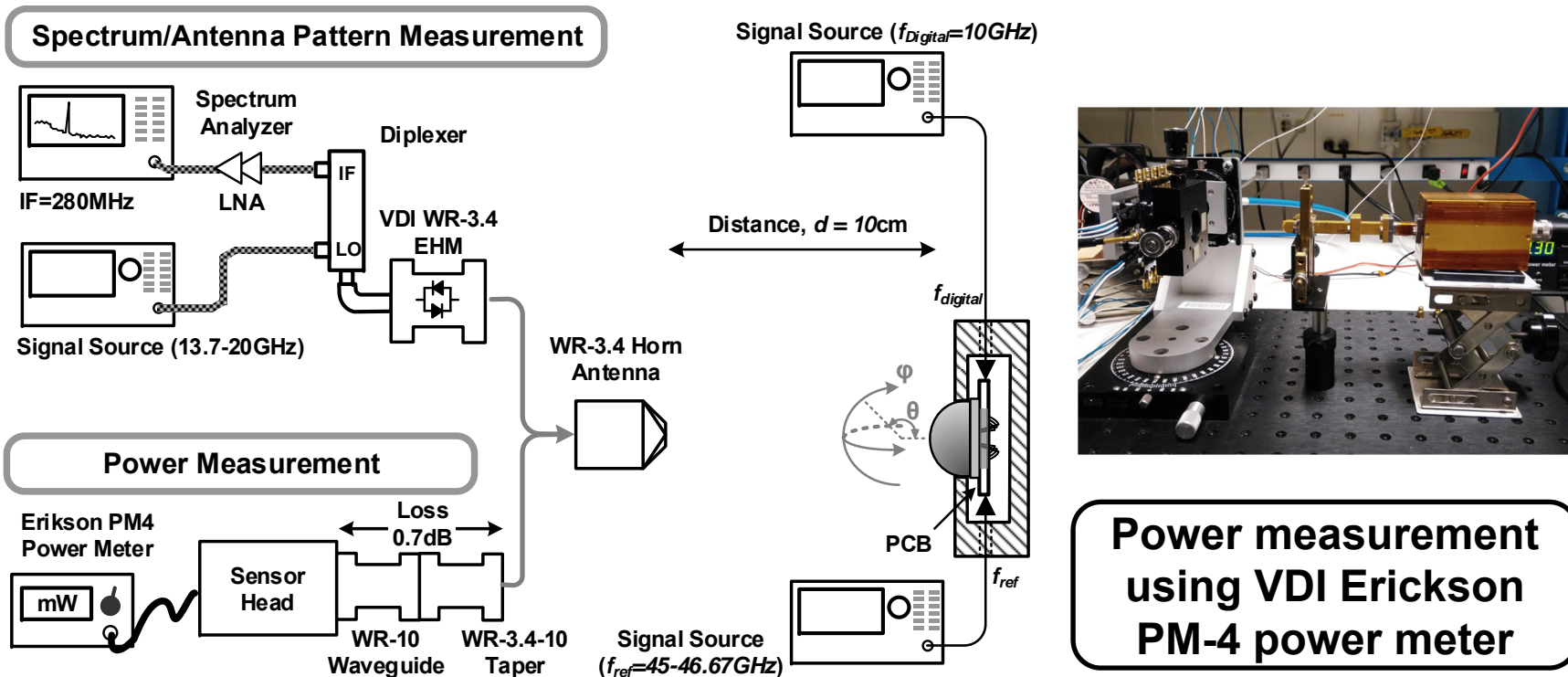
Chip Micrograph and Packaging



**Chip bonded on PCB
with hemispheric
silicon lens**

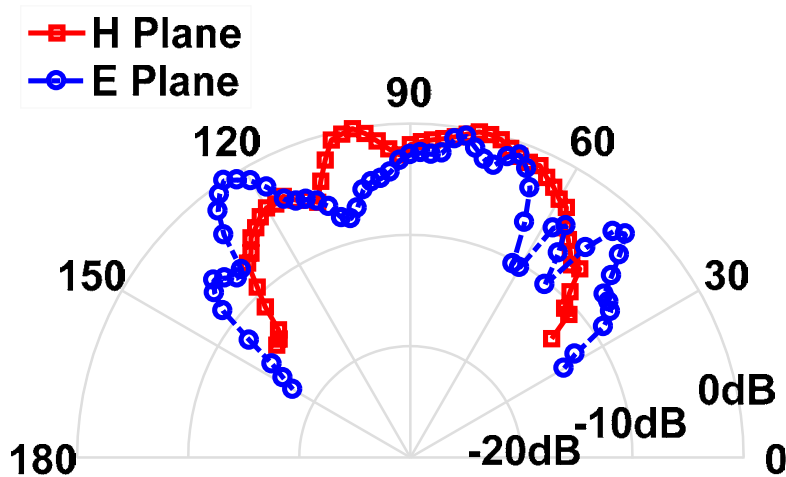
- **TSMC 65nm bulk CMOS process**
- **Chip area: 2mm × 3mm**
- **DC power consumption: 1.7W**

Measurement Setup of TX Mode

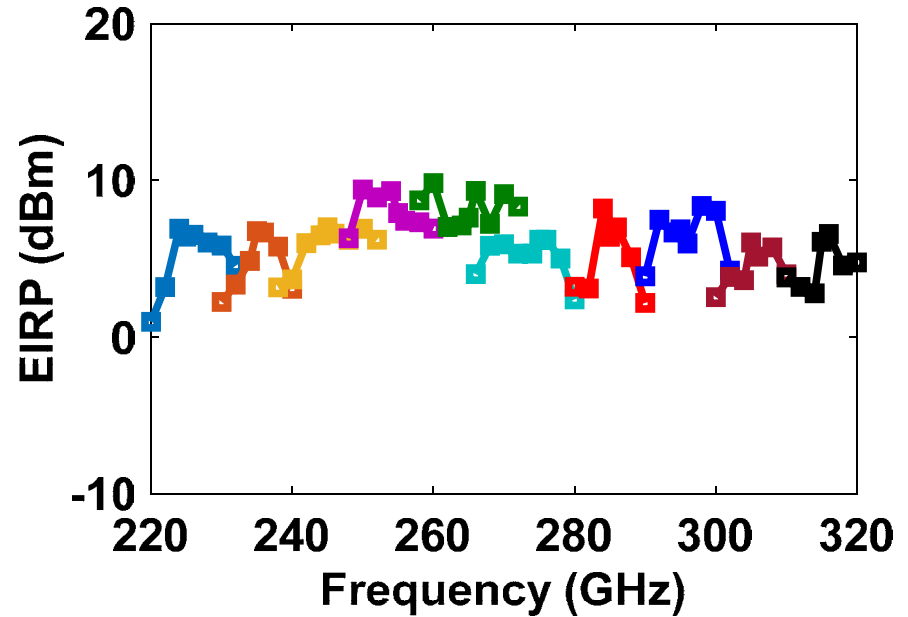


- For power measurement, only one AMP is turned on at each time

Measurement Results of TX Mode



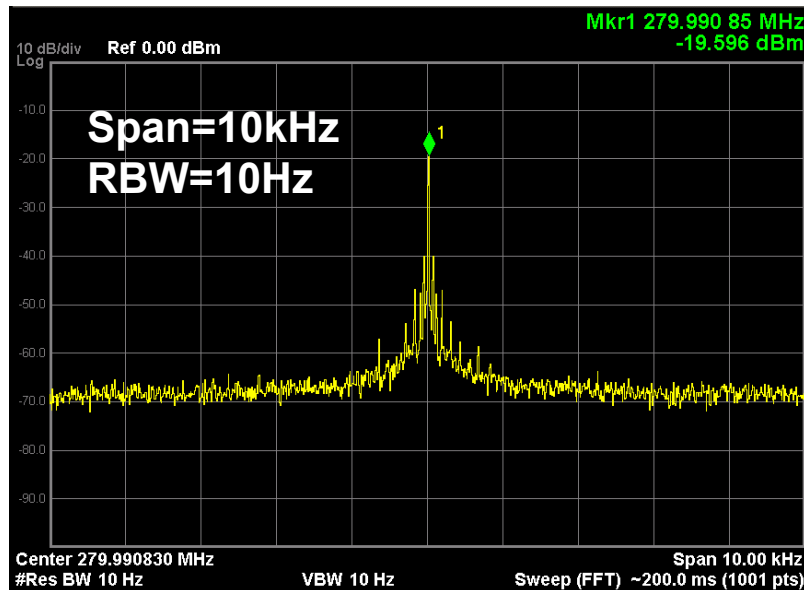
Antenna pattern of a comb line at 265GHz



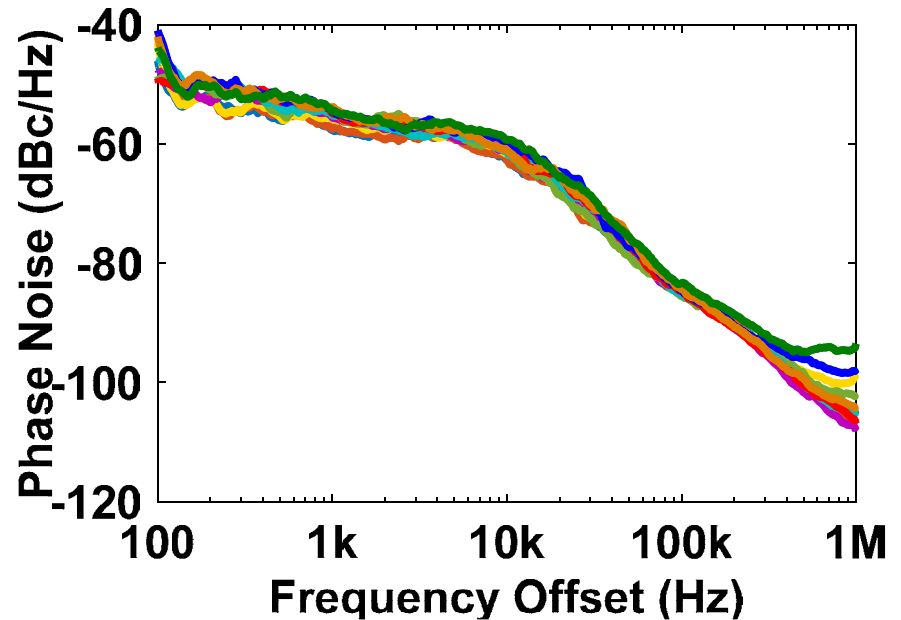
Equivalent isotropic radiated power (EIRP)

- Total radiated power of 10 comb lines: 5.2mW

Measurement Results of TX Mode



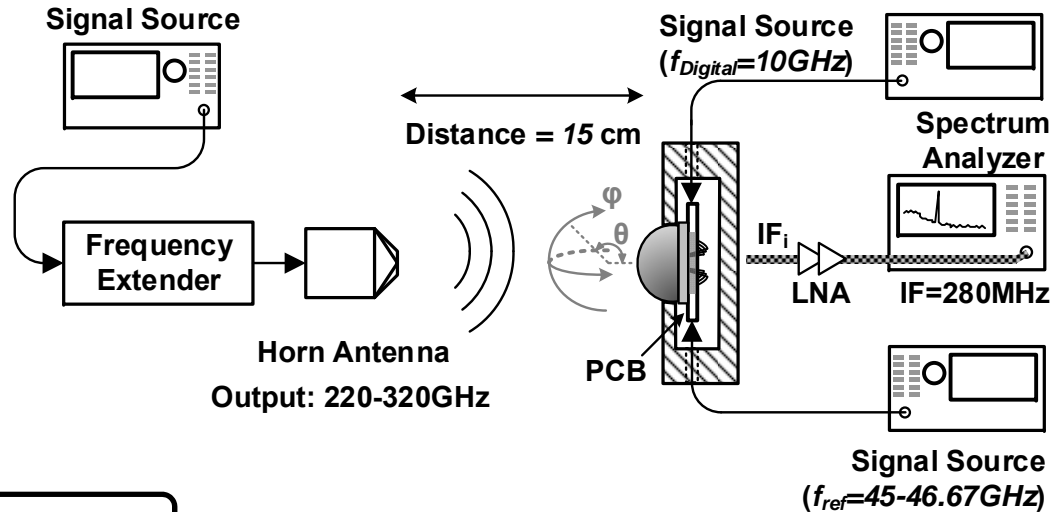
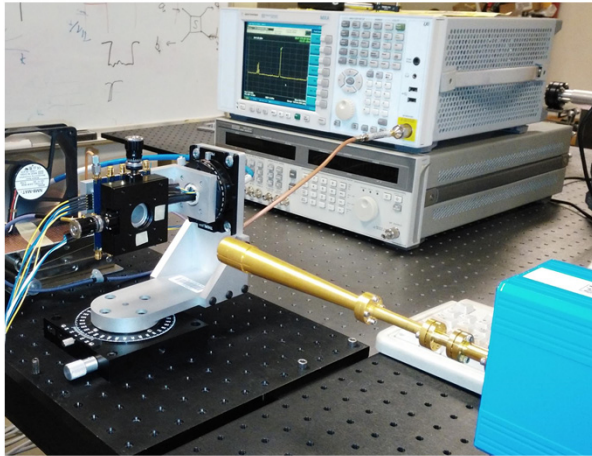
Spectrum of a comb line
at 265GHz



Phase noise of 10 comb
lines

- Average measured phase noise for 10 comb lines at 1MHz offset: -102dBc/Hz

Measurement Setup of RX Mode



Single-sideband conversion gain

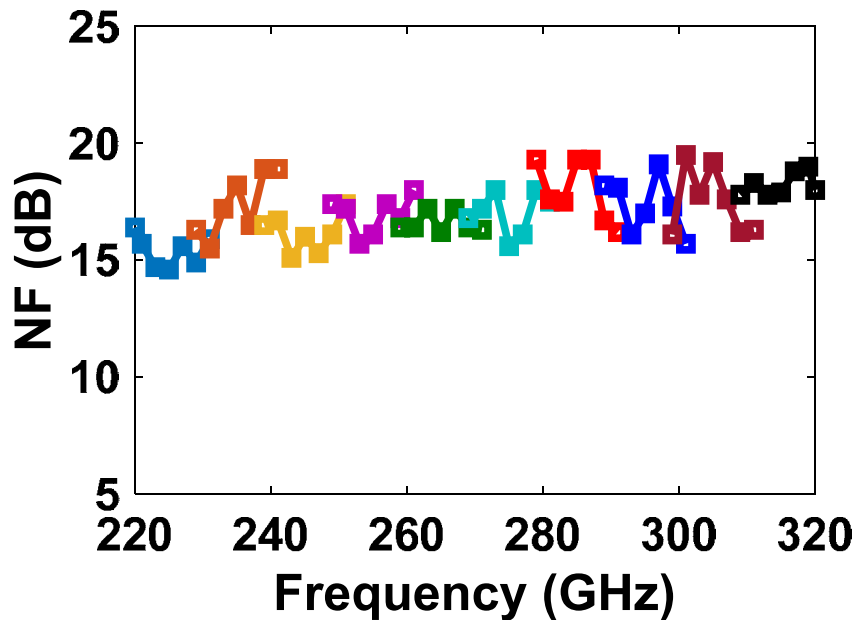
$$CG = \frac{\text{IF output power}}{\text{Power received by RX antenna aperture}}$$

$$= \text{IF output power (dBm)} - (\text{TX power (dBm)} + \text{TX antenna gain (dB)} - \text{Path loss (dB)} + \text{RX antenna directivity (dB)})$$

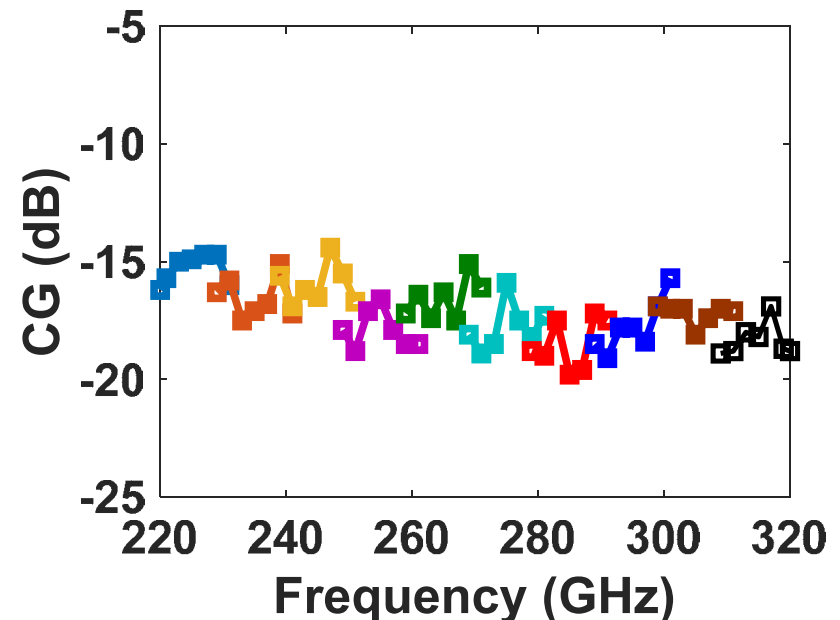
Single-sideband noise figure (antenna loss incorporated)

$$NF = \text{IF noise floor (dBm/Hz)} - (-174 \text{ (dBm/Hz)}) - CG \text{ (dB)}$$

Measurement Results of RX Mode



Single-sideband noise figure



Single-sideband conversion gain

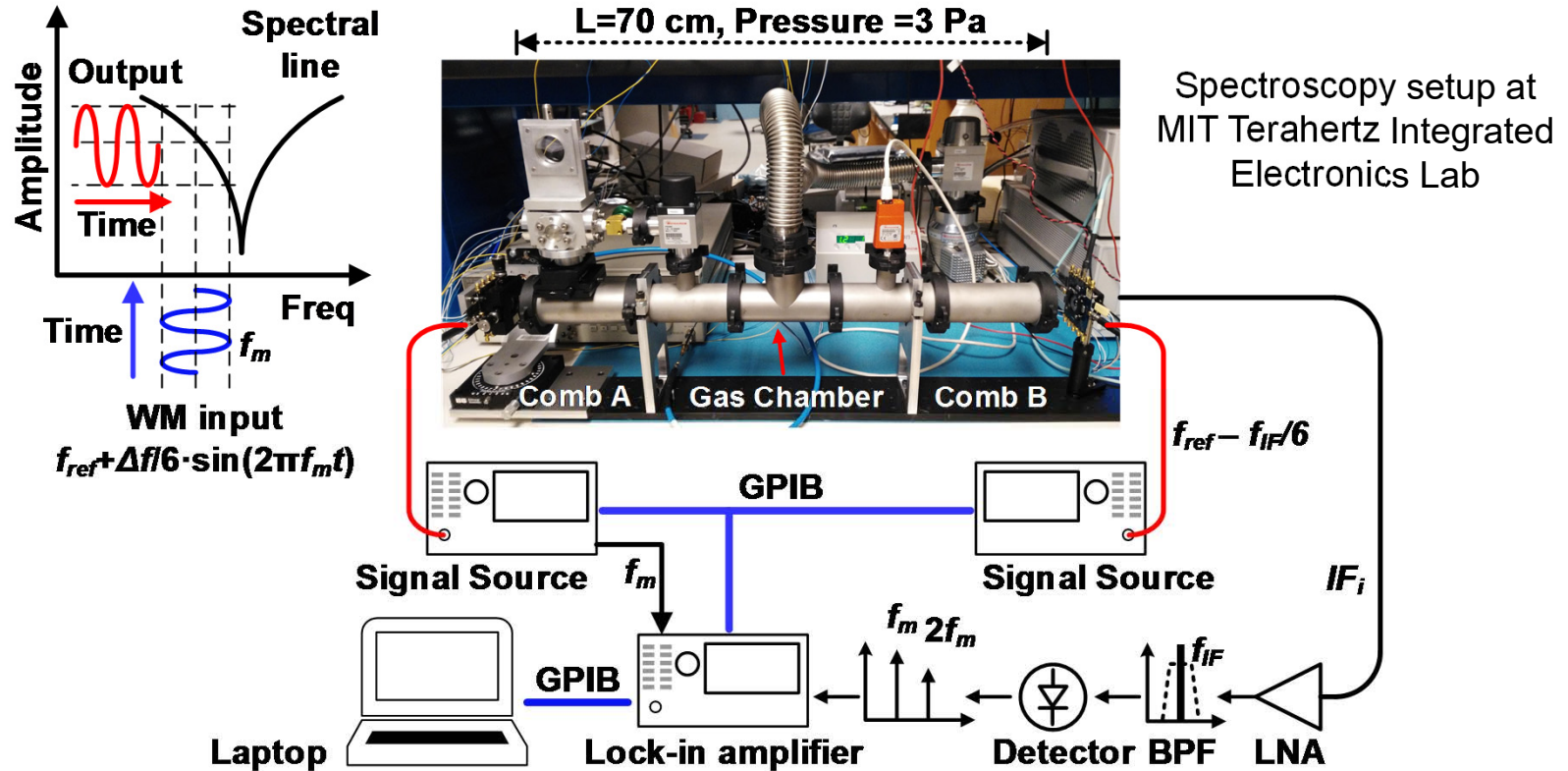
- Measured SSB noise figure: 14.6~19.5dB

Performance Comparison Table

Ref.	Technology (f_{\max})	Topology	Frequency (GHz)	BW (GHz)	P_{radiated} (mW)	Phase Noise ¹ (dBc/Hz)	Noise Figure (dB)	P_{DC} (W)
This work	65nm CMOS (250GHz)	Comb (Tx/Rx)	220~320	100	5.2	-102	14.6~19.5	1.7
TST2016	0.13 μm SiGe (500GHz)	Tx+Rx	245	14	4.0	-85	18	1.5+0.6 (Tx+Rx)
JSSC2014	32nm CMOS (320GHz)	Tx+Rx	210	14	0.7 ²	-81	11~12 ³	0.24+0.086 (Tx+Rx)
VLSI2016	65nm CMOS (N/A)	Tx	208~255	47	0.1 ⁴	-80	N/A	1.4
JSSC2015	0.13 μm SiGe (280GHz)	Tx	317	N/A	3.3	-79	N/A	0.61
ISSCC2016	65nm CMOS (N/A)	Rx	210~305	95	N/A	N/A	18.4~23.5 ⁵ (NF _{ISO} =13.9~19)	N/A

- 1 MHz frequency offset.
- The P_{radiated} is estimated from the PA output power of 2.9 mW, and the antenna loss of 6 dB.
- The NF of low noise amplifier in the receiver, excluding on-chip antenna loss.
- The reported power in [3] is EIRP, not the total radiated power.
- The overall NF (18.4~23.5 dB) = NF_{ISO}(13.9~19 dB, Isotropic Noise Figure)- (Antenna Loss (~4 dB) + Antenna Gain (-1~2 dBi)) .

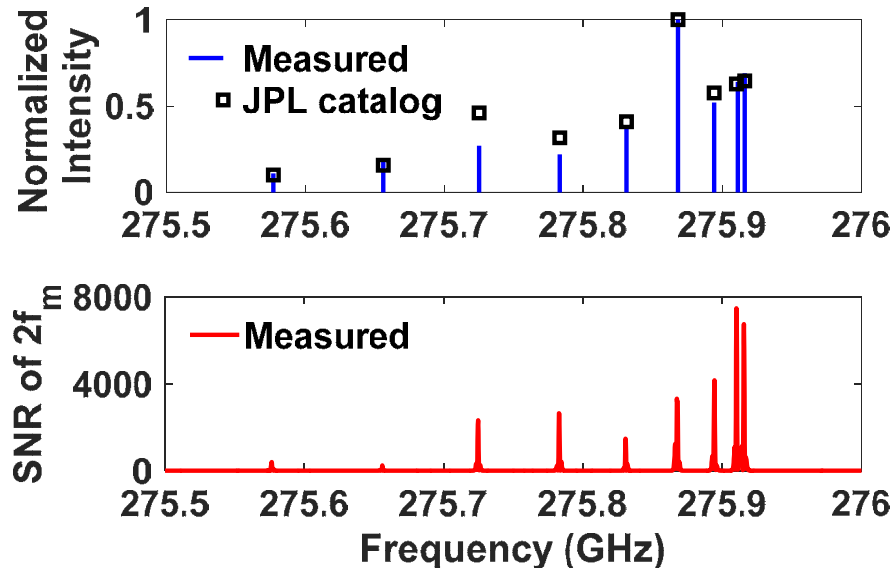
Spectroscopy Demonstration Setup



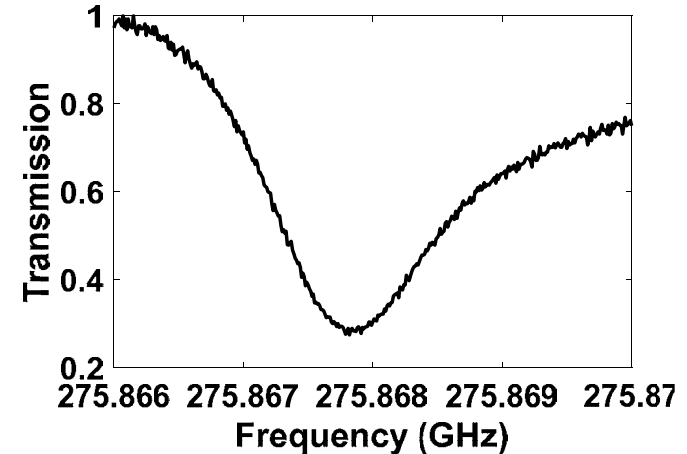
- Wavelength modulation (WM) is applied for reduced impacts due to standing-wave formation
 - $\Delta f = 240\text{kHz}$, $f_m = 50\text{kHz}$, $f_{IF} = 950\text{MHz}$

Spectrum of Acetonitrile (CH₃CN)

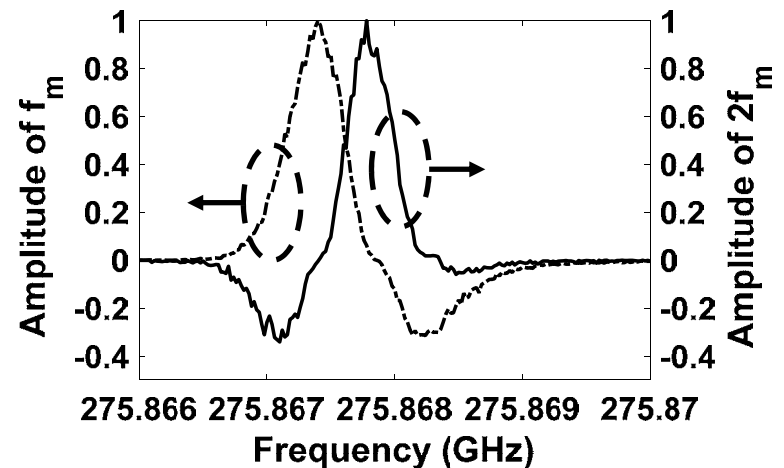
Measured spectrum of CH₃CN



Spectral line w/o WM



Spectral line with WM



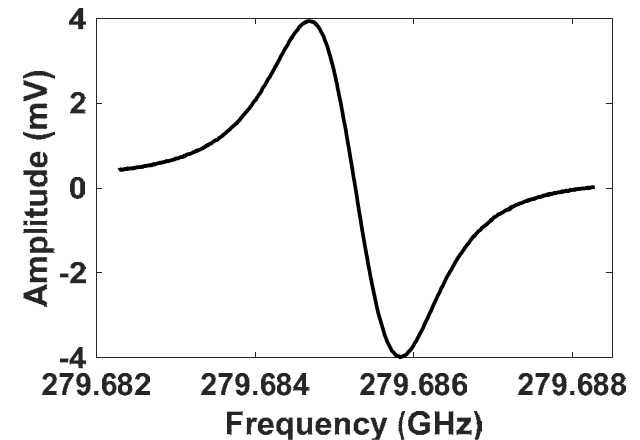
- Measurement matches the JPL molecular database
- Spectral linewidth of 380kHz is obtained
 - Absolute specificity ($Q=7 \times 10^5$)

[JPL Molecular Spectroscopy, spec.jpl.nasa.gov.]

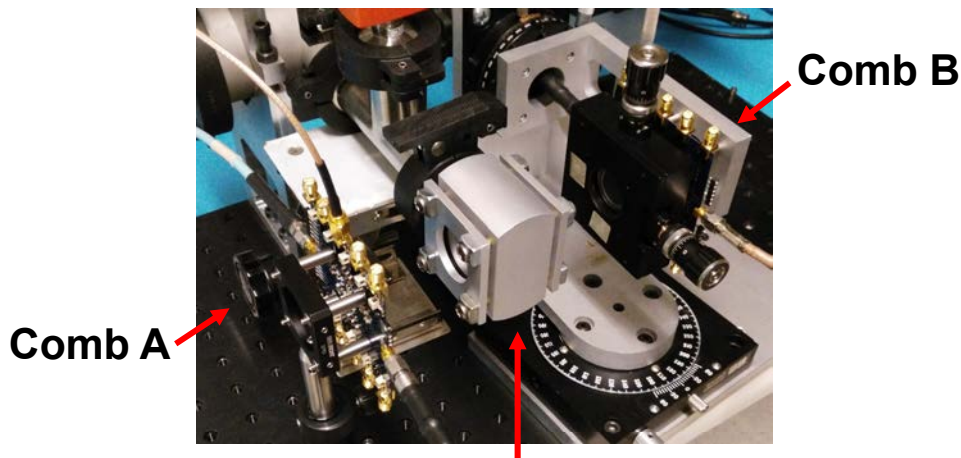
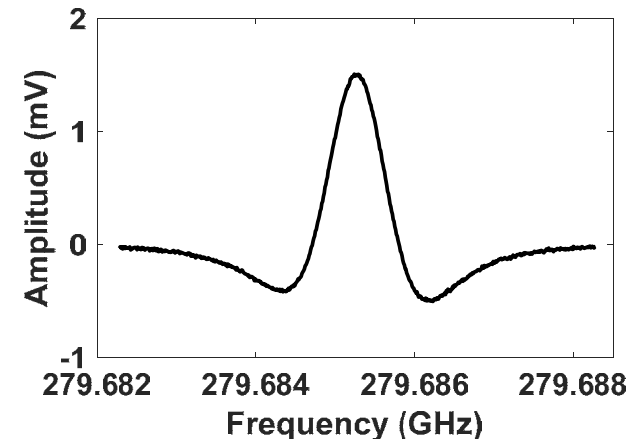
Spectrometer Miniaturization

- **54dB SNR has been achieved with reduced gas cell size**
 - Compact 3cm-long gas cell
 - Sample: carbonyl sulfide (OCS), 1.21×10^{-21} cm integrated line intensity (JPL) at 279.685GHz
 - Integration time: 100ms

1st order derivative, SNR=54dB



2nd order derivative, SNR=44dB



3cm-long gas cell

Outline

- Background
- Dual-Frequency-Comb Spectroscopy
- Architecture and Circuit Design
- Measurement Results
- **Conclusions**

Conclusions

- **Architecture level: Dual-frequency-comb spectroscopy with $>2N\times$ ($N=10$) faster frequency scanning and lower total energy consumption**
 - Simultaneous bilateral transmit/receive
- **Circuit level: multi-functional active molecule probe (AMP), performing frequency doubler, sub-harmonic mixer and on-chip antenna simultaneously**
 - Proposed dual-transmission-line (DTL) feedback accurately achieves G_{max}
- **Prototype: 220-to-320GHz comb spectrometer with state-of-the-art 5.2mW radiated power and 14.6-to-19.5dB NF**
 - Spectroscopy demonstration with 3-cm gas cell and a SNR of 54dB

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