



## RTU2B-2

# Fully-Scalable 2D THz Radiating Array: A 42-Element Source in 130-nm SiGe with 80- $\mu$ W Total Radiated Power at 1.01THz

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## Outline

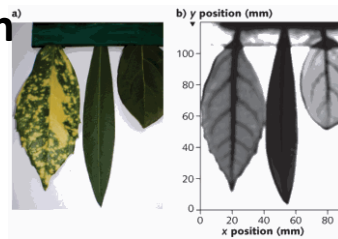
- **Motivation and Challenges**
- **Design of Oscillator**
- **Formation of 1-THz Oscillating-Radiating Array**
- **Measurement Results**
- **Conclusions**

## Pushing Frequency and Power Limit of THz Radiator

### Applications of high-power high-frequency THz source

#### High-Resolution Imaging

[F. Schuster et al., ISSCC, 2011.]



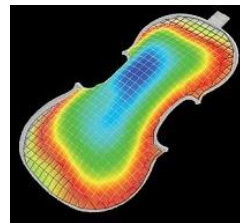
#### Bio-Molecule Spectroscopy

[T. Globus et al., *Convergent Science Physical Oncology*, 2016.]

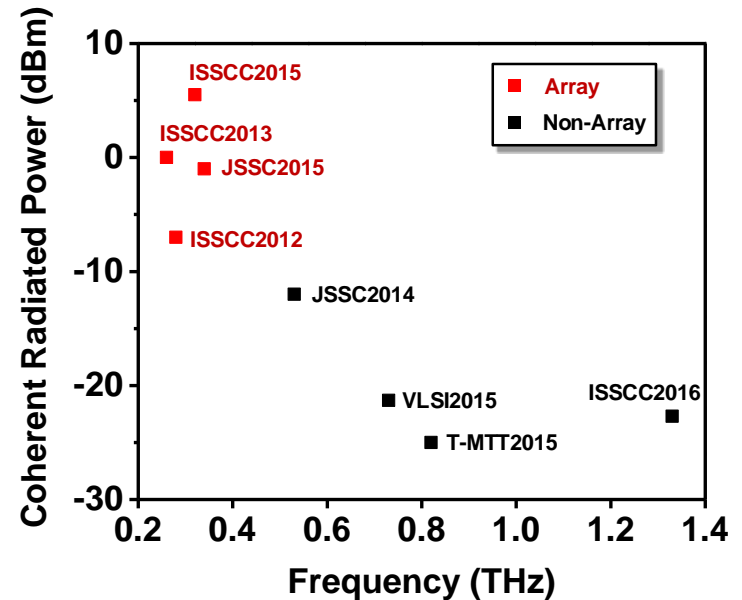


#### High-Precision Vibrometry

[G. Bissinger, D. Oliver, *Sound & Vibration*, 2007.]



### Path to high-power 1-THz radiator



- Building coherent radiating array at higher frequency is more challenging

# Why Building 1-THz Radiating Array Is Difficult?

1 THz  $>$   $f_{\max}$  of all silicon-based transistors (fastest: 450 GHz in IHP S13G2)



Efficient high-order harmonic generation and radiation

Antenna array requires  $\lambda/2$  spacing



$\sim 70\mu\text{m} \times 70\mu\text{m}$  for each radiating unit



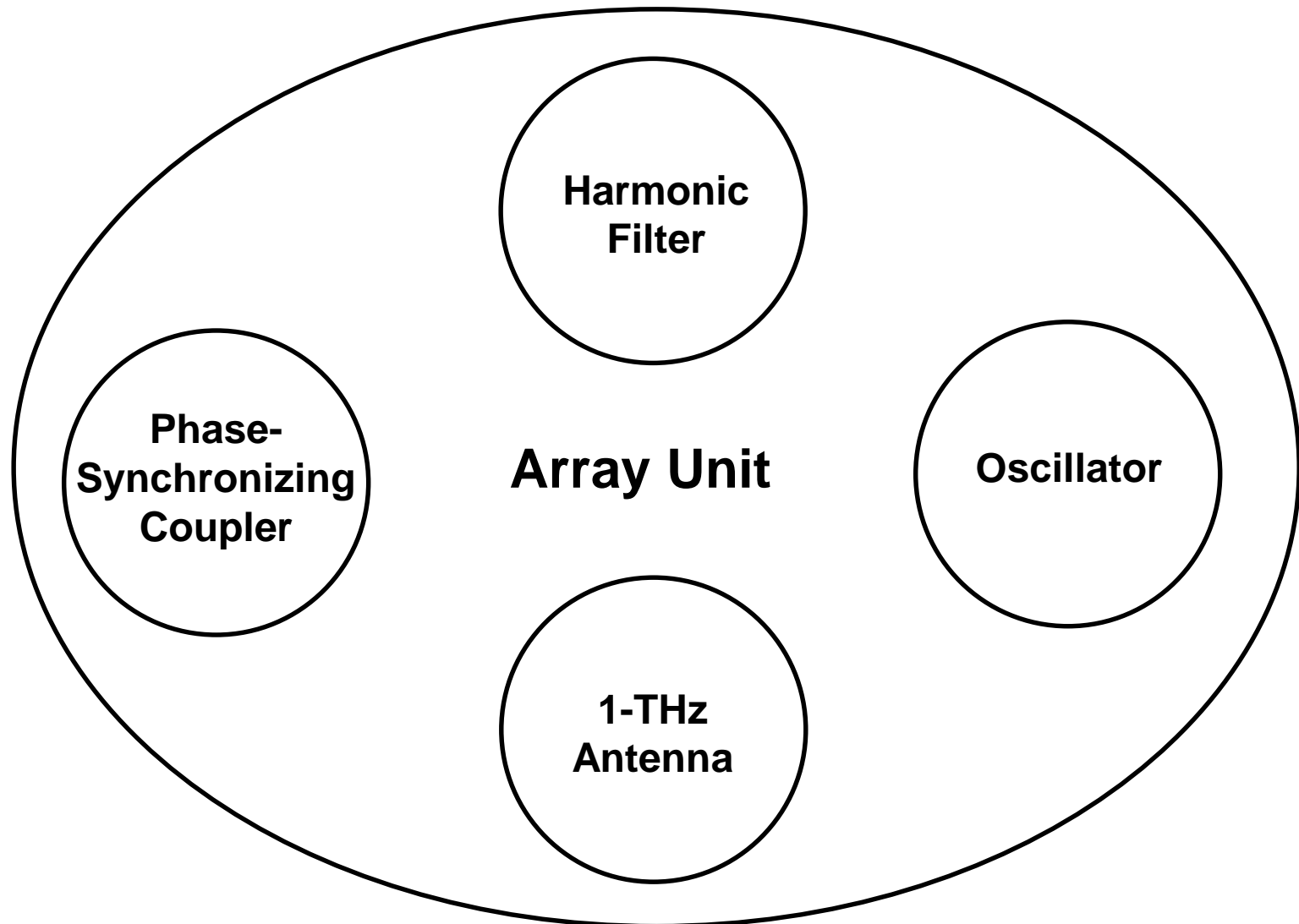
Very limited area to fit in all necessary components

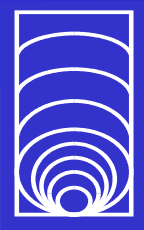
Array scale can be very large



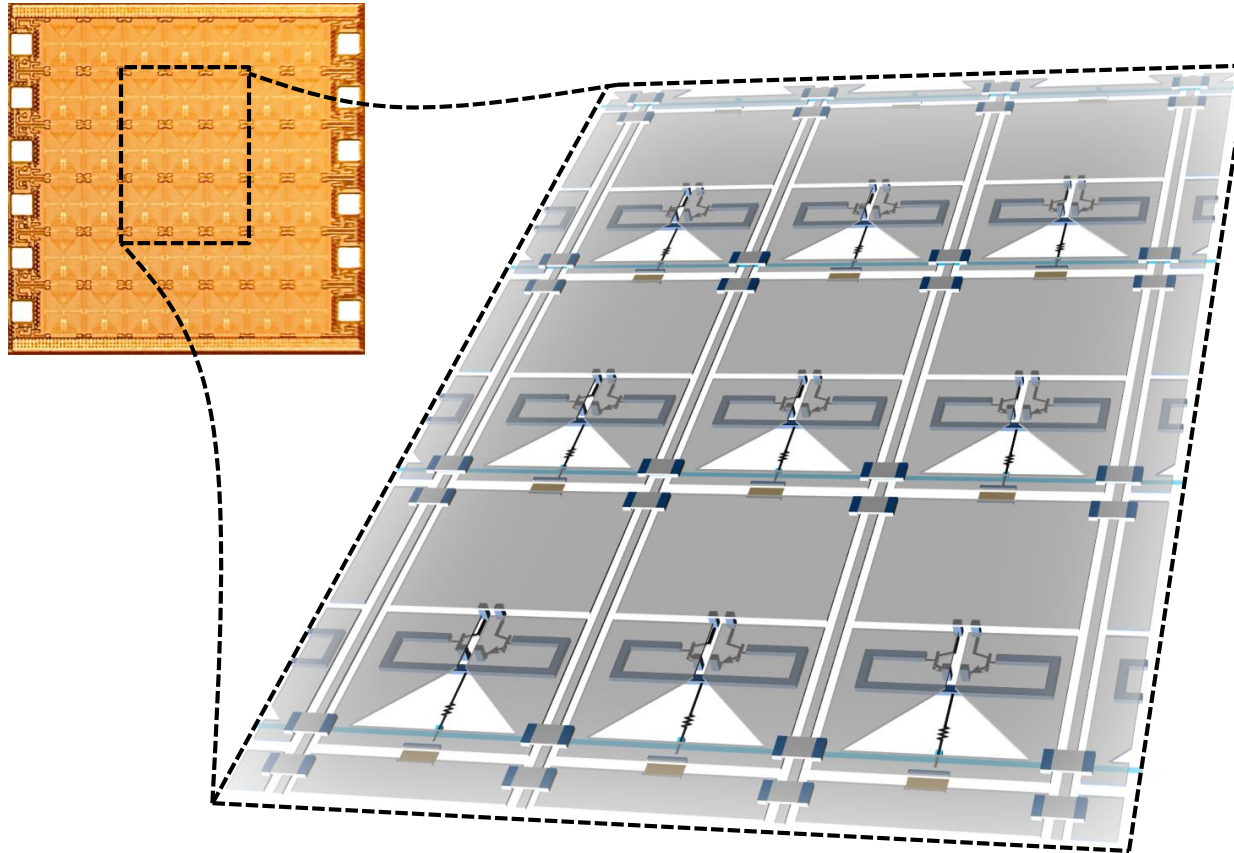
Accumulation of phase error between units due to inter-unit injection can cause severe beam tilting

# Call for Compact Multi-Functional Array Unit





## Our Slotline-Bound-Array Solution



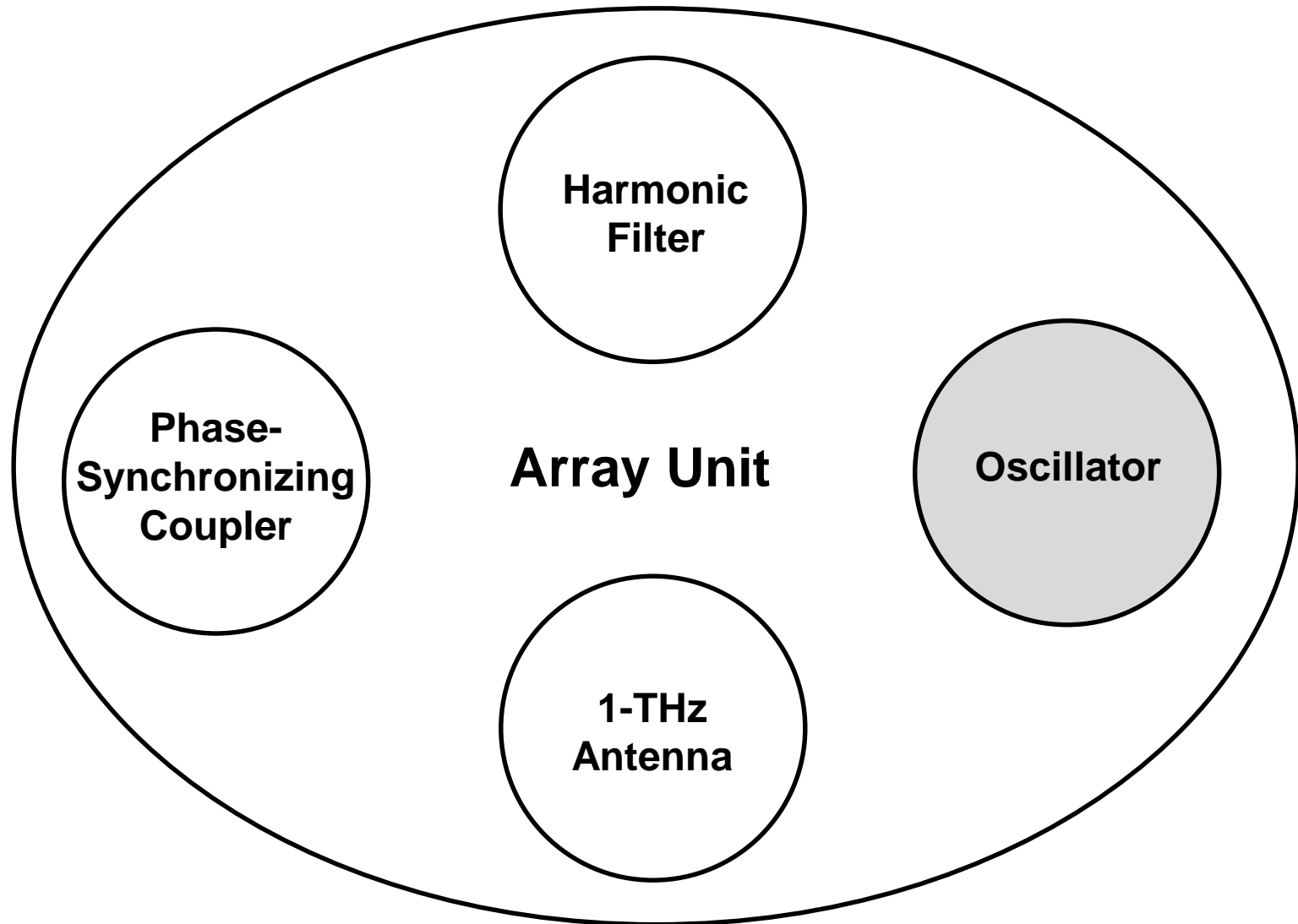
- **Differential oscillators plus slotlines accomplish all tasks**
  - Each unit oscillates at  $f_0 = 250$  GHz and radiates  $4f_0 = 1$  THz



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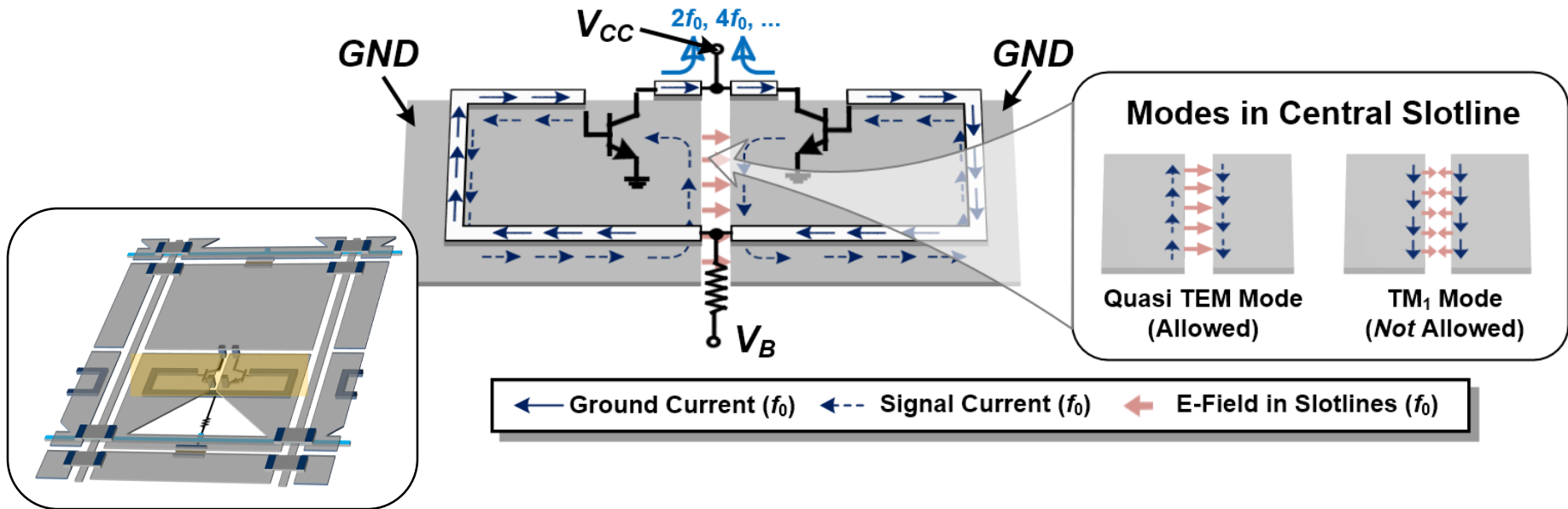
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# Multi-Functional Array Unit



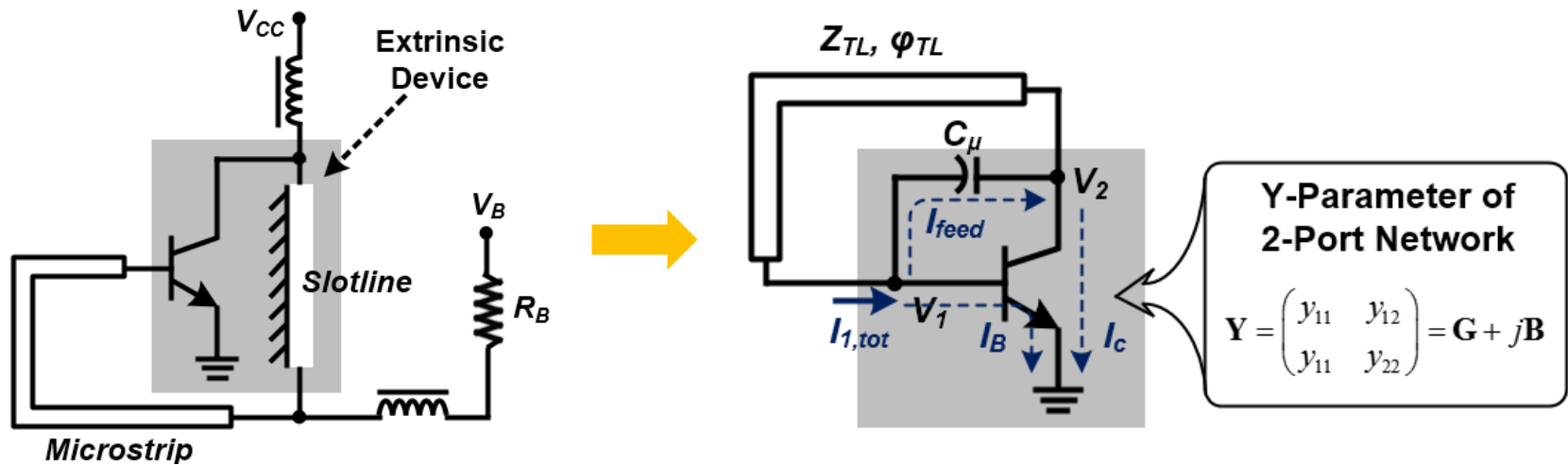


# Oscillator Pair Capable of Efficient Harmonic Generation



- At  $f_0$  (250 GHz), two oscillators are forced to oscillate differentially
- For even-order harmonics from two oscillators, including  $4f_0 = 1$  THz
  - They are in-phase, hence repelled from slotline (feedback loop)
  - No dissipation at base, more power is delivered outwards

## Maximize Oscillation at $f_0$ in Single Oscillator

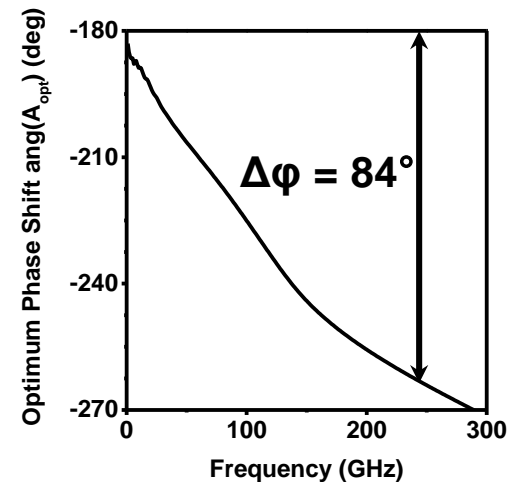


- **Phase delay of  $V_2$  should be compensated**
  - Intrinsic delay of  $I_C$
  - Undesired feed-forward current  $I_{feed}$
- **Use self-feeding topology to adjust phase**

$$\angle A_{opt} = \angle V_2 / V_1 = -(y_{21} + y_{12}^*),$$

$$\varphi_{TL} = \arcsin \left( Z_{TL} \cdot \left( g_{11} + \operatorname{Re} \left( A_{opt} \cdot y_{12} / \operatorname{Im}(A) \right) \right) \right)^{-1}$$

[R. Spence, Linear Active Networks, 1970.]

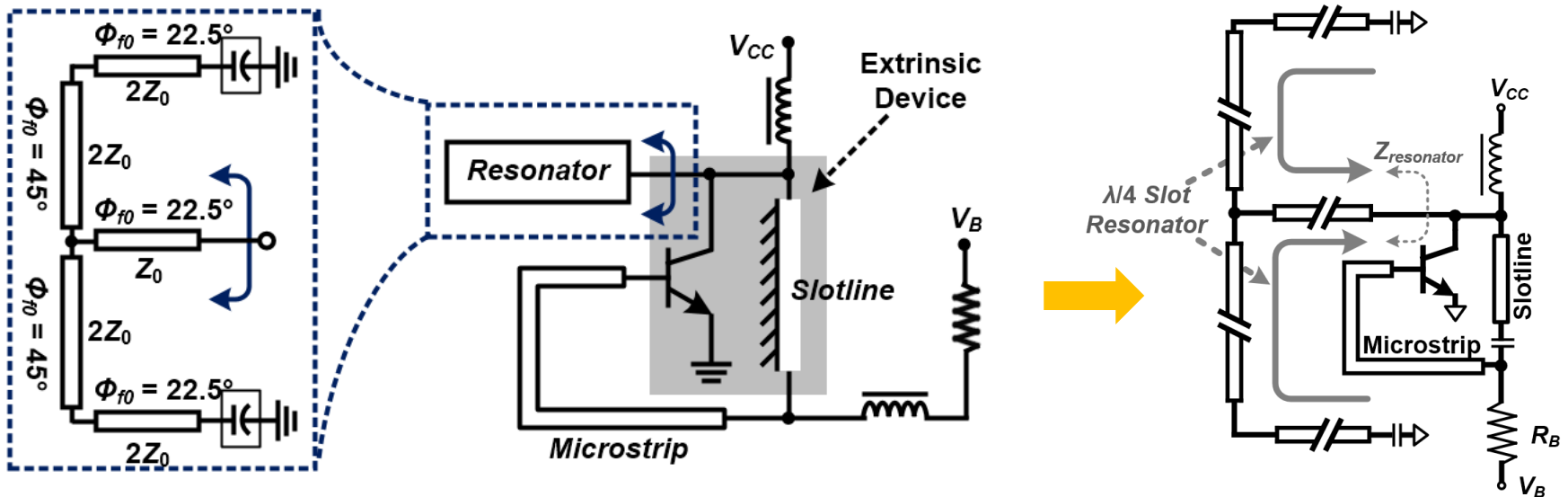




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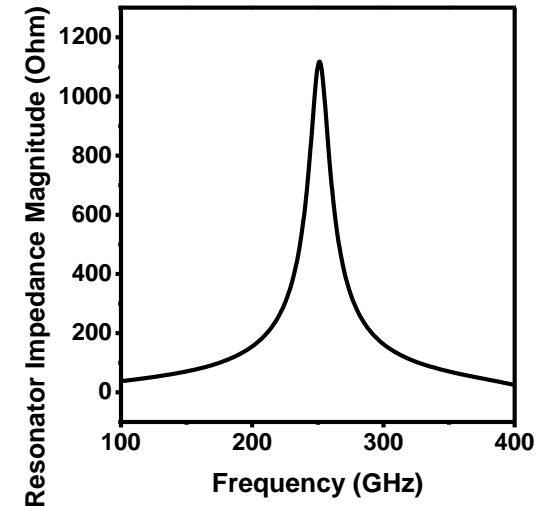
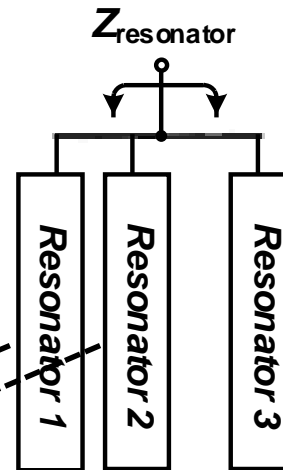
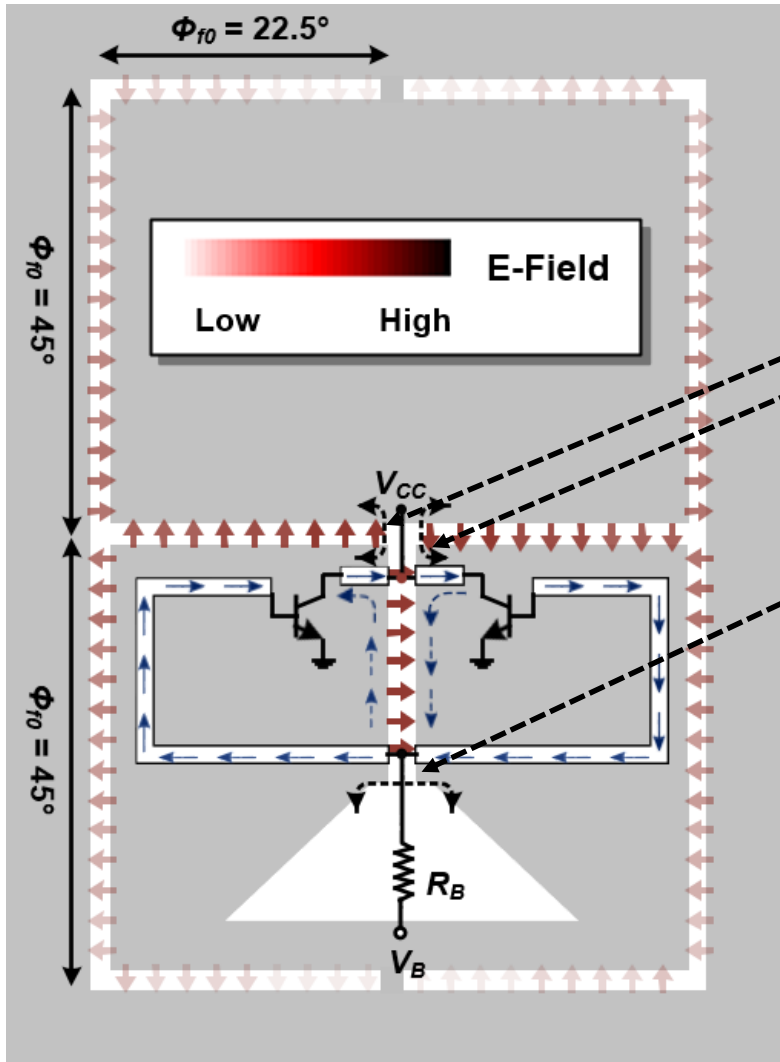
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## Expose Oscillation Using Branched Resonator



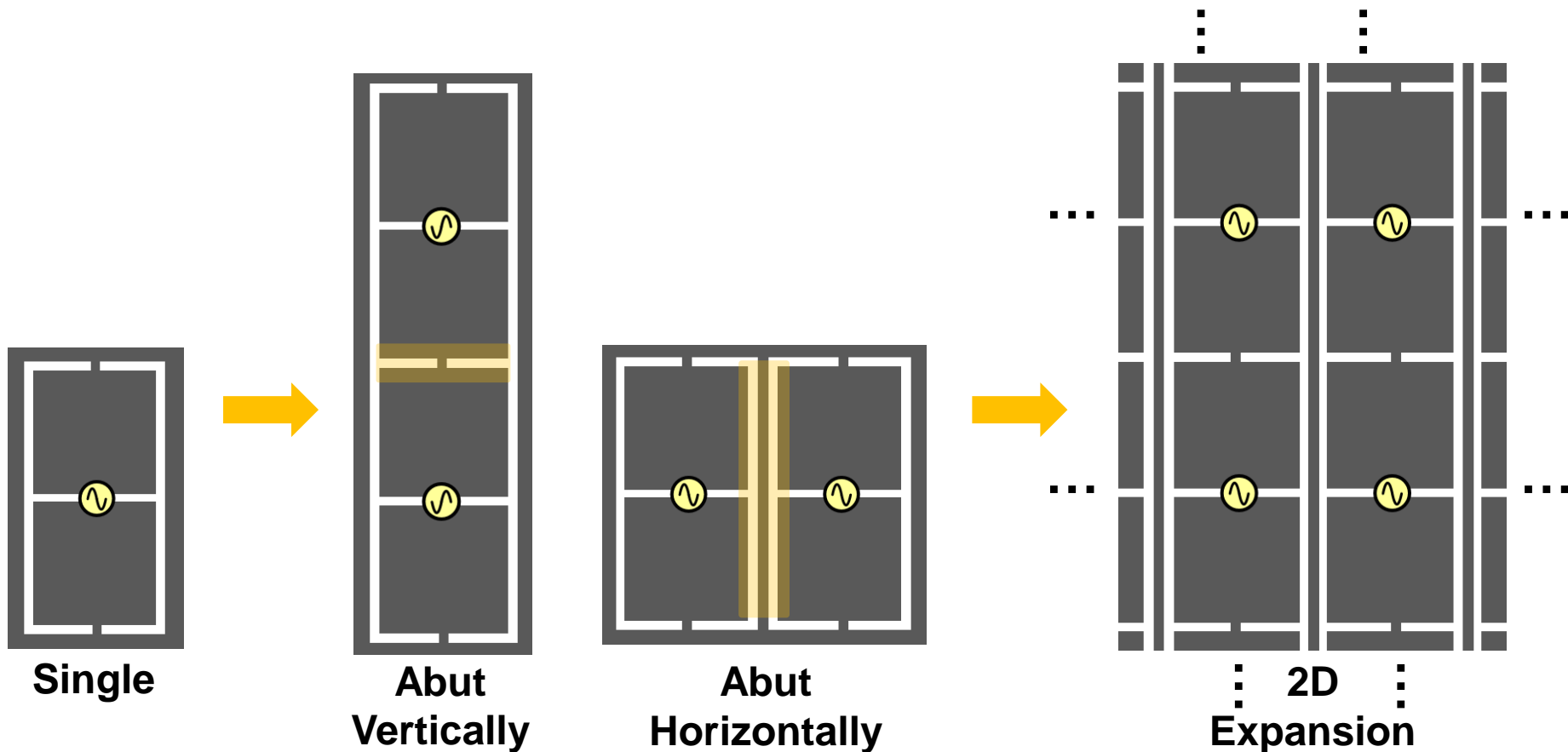
- Two  $\lambda/4 @ f_0$  transmission lines (short  $\rightarrow$  open)
- E-shaped pattern composes the boundary of oscillating unit
- Resonator is implemented by slotlines

## Structure of a Complete Oscillating Unit



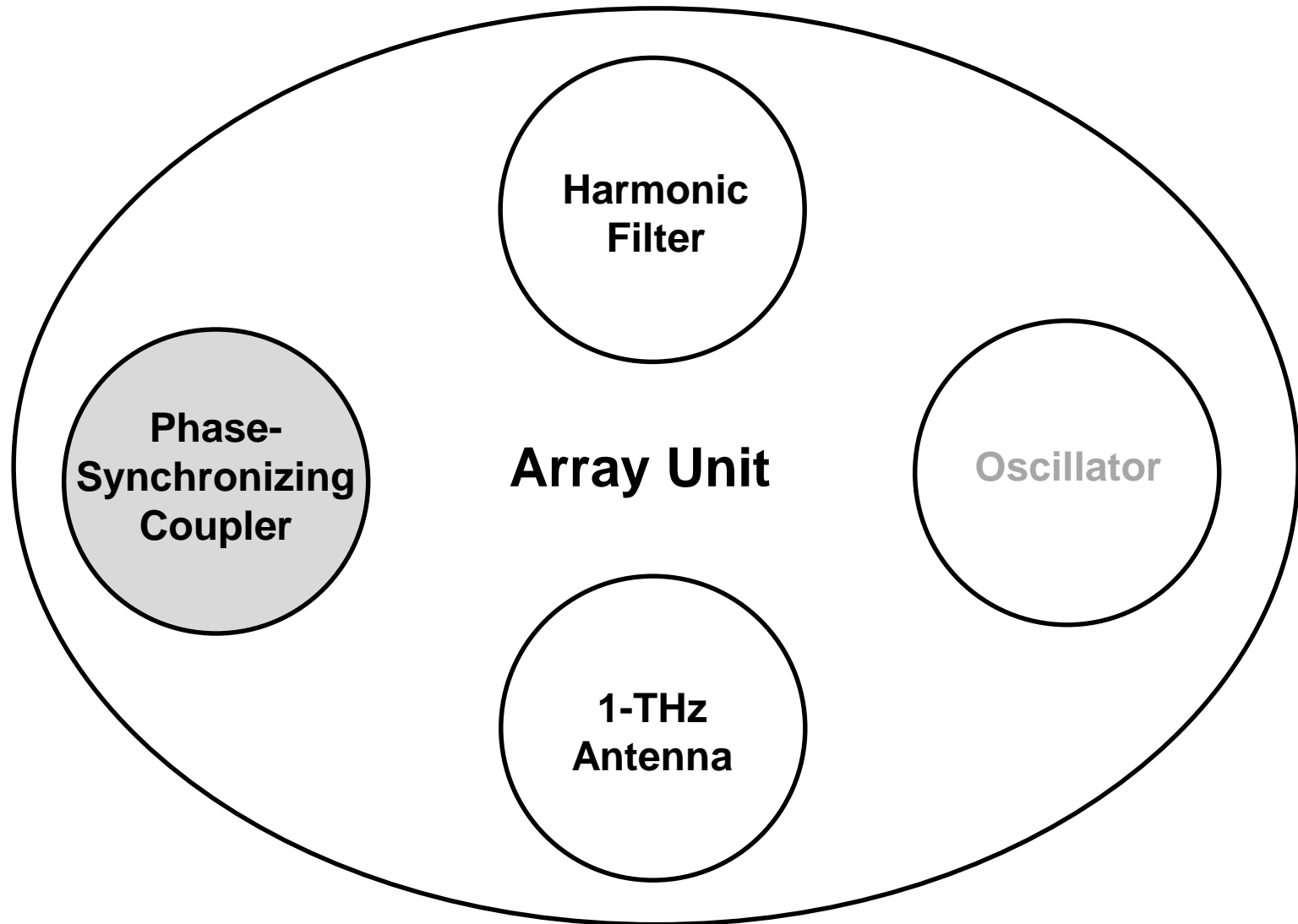
- **Oscillators sealed by three resonators**
  - Two branched resonators
  - One broadband open
- **In-shunt resonators present  $Q = 18$**

## Interface Adjacent Units Using Branched Resonator

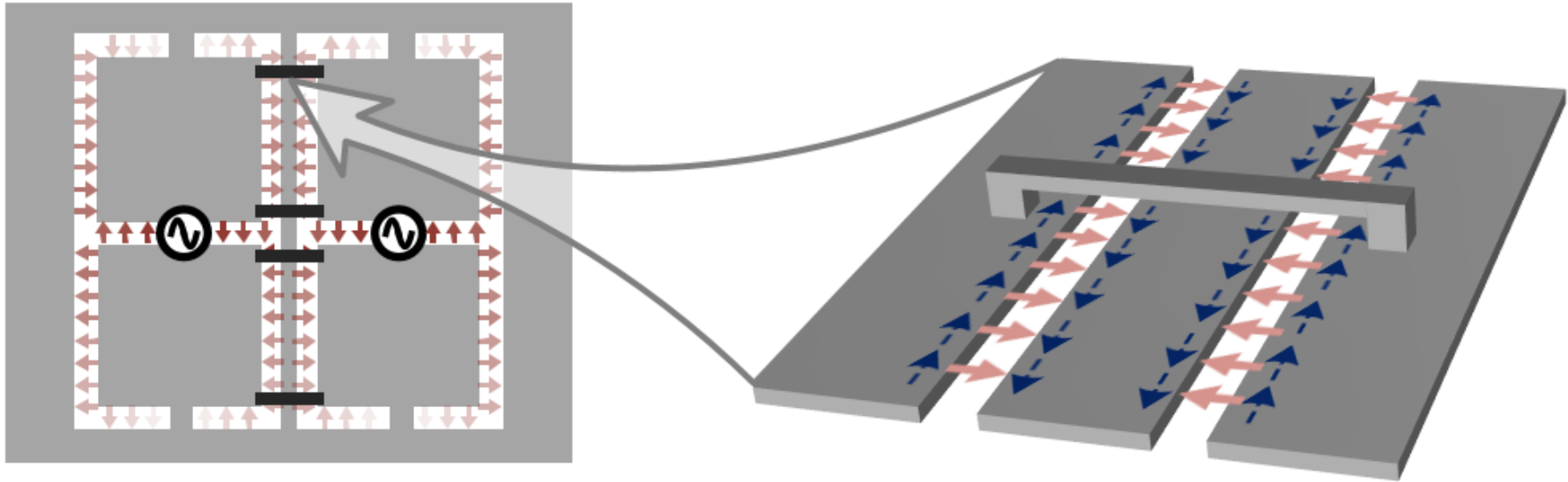


- Horizontal slotlines on the border (2x1 case) are merged
- Vertical slotlines on the border (1x2 case) run parallel

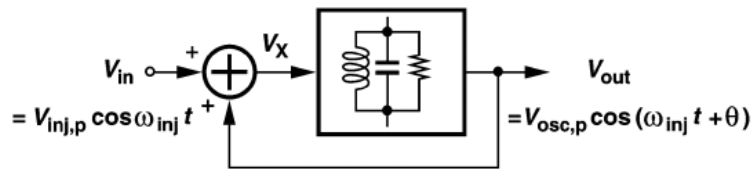
## Multi-Functional Array Unit



## Coupling (at $f_0$ ) between Horizontally Adjacent Units

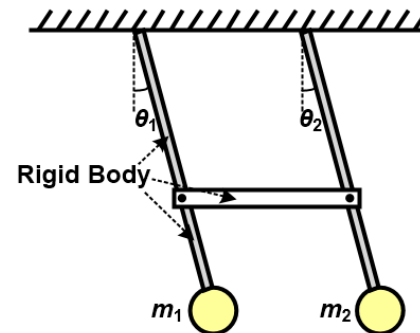


### Single-Node Injection vs. Distributed Phase Synchronization



$$\boxed{\frac{d\theta}{dt}} = \omega_0 - \omega_{inj} - \frac{\omega_0}{2Q} \cdot \frac{V_{inj,p}}{V_{osc,p}} \sin \theta$$

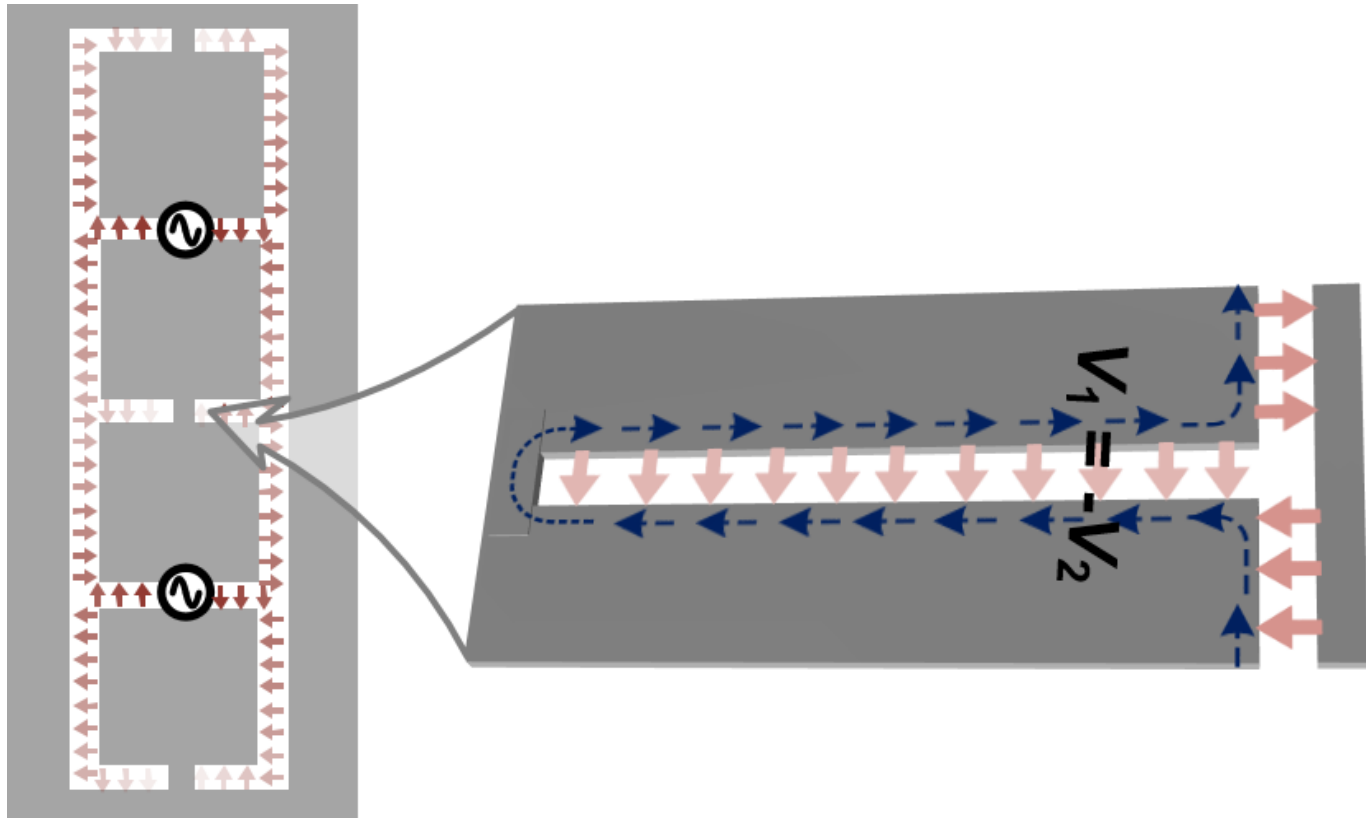
$$= \omega_0 - \omega_{inj} - \omega_L \sin \theta.$$



Phase at every point is synced, even if there is mismatch of  $\omega_0$

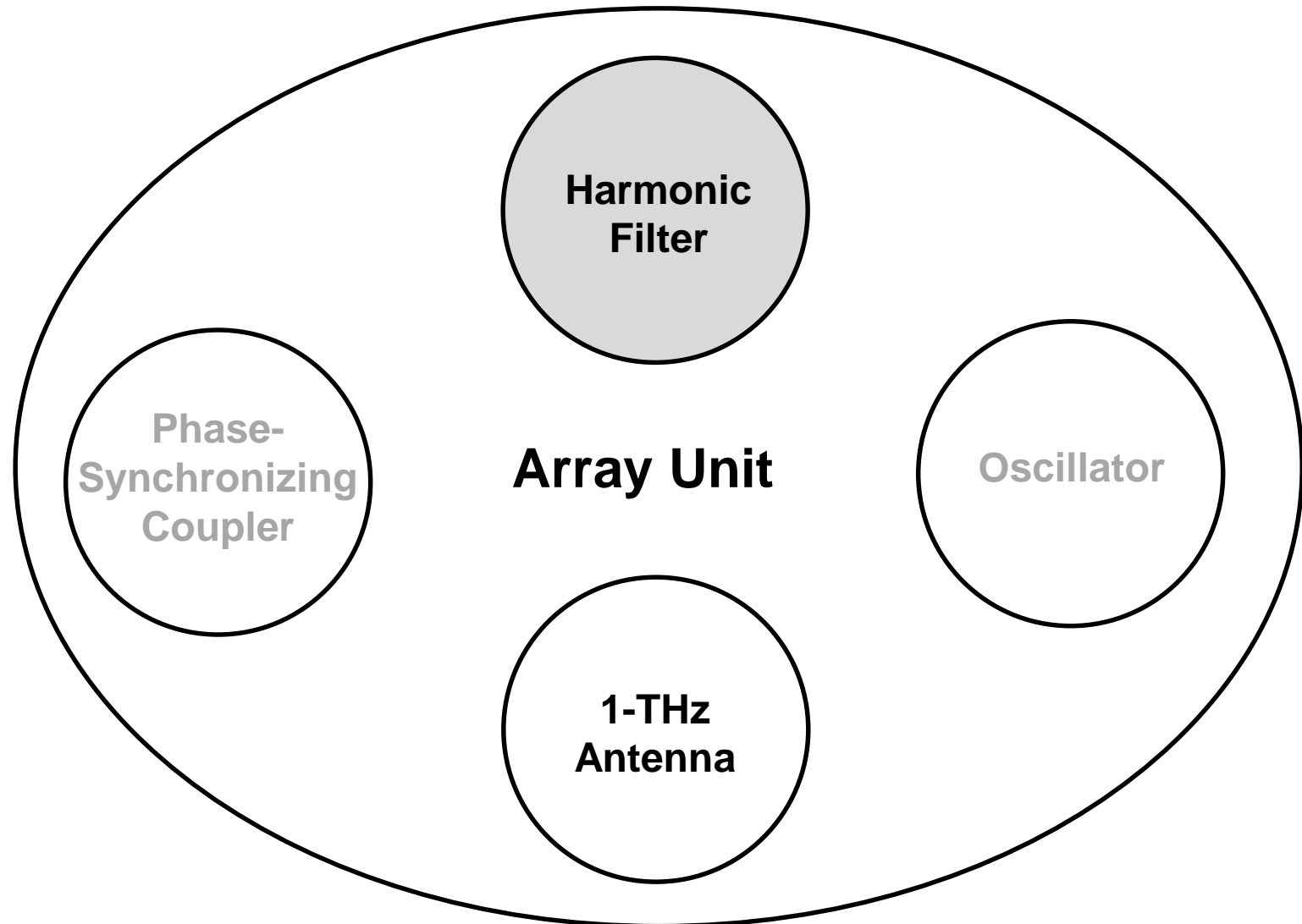


## Coupling (at $f_0$ ) between Vertically Adjacent Units



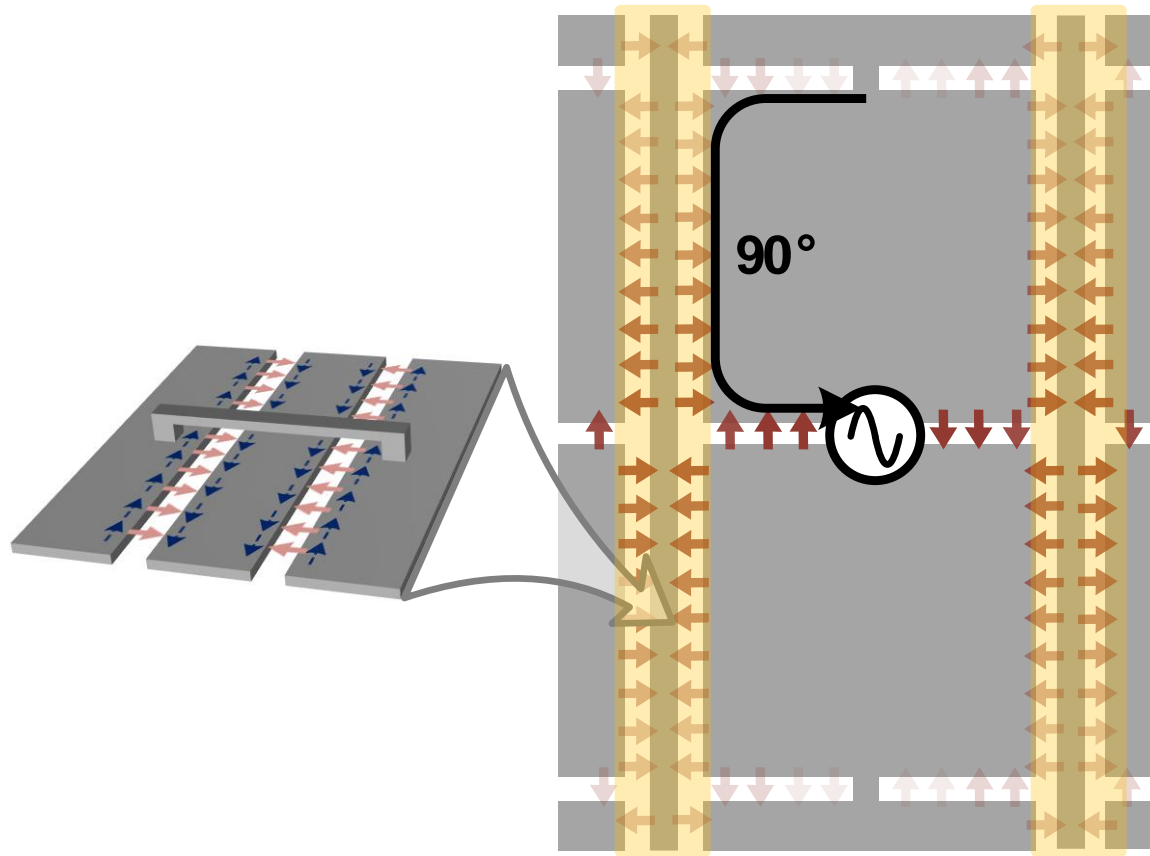
- Branched resonator shared  $\rightarrow$  phase relationship determined
- Use slotline for the purpose of array-wide in-phase radiation (discuss later)

## Multi-Functional Array Unit



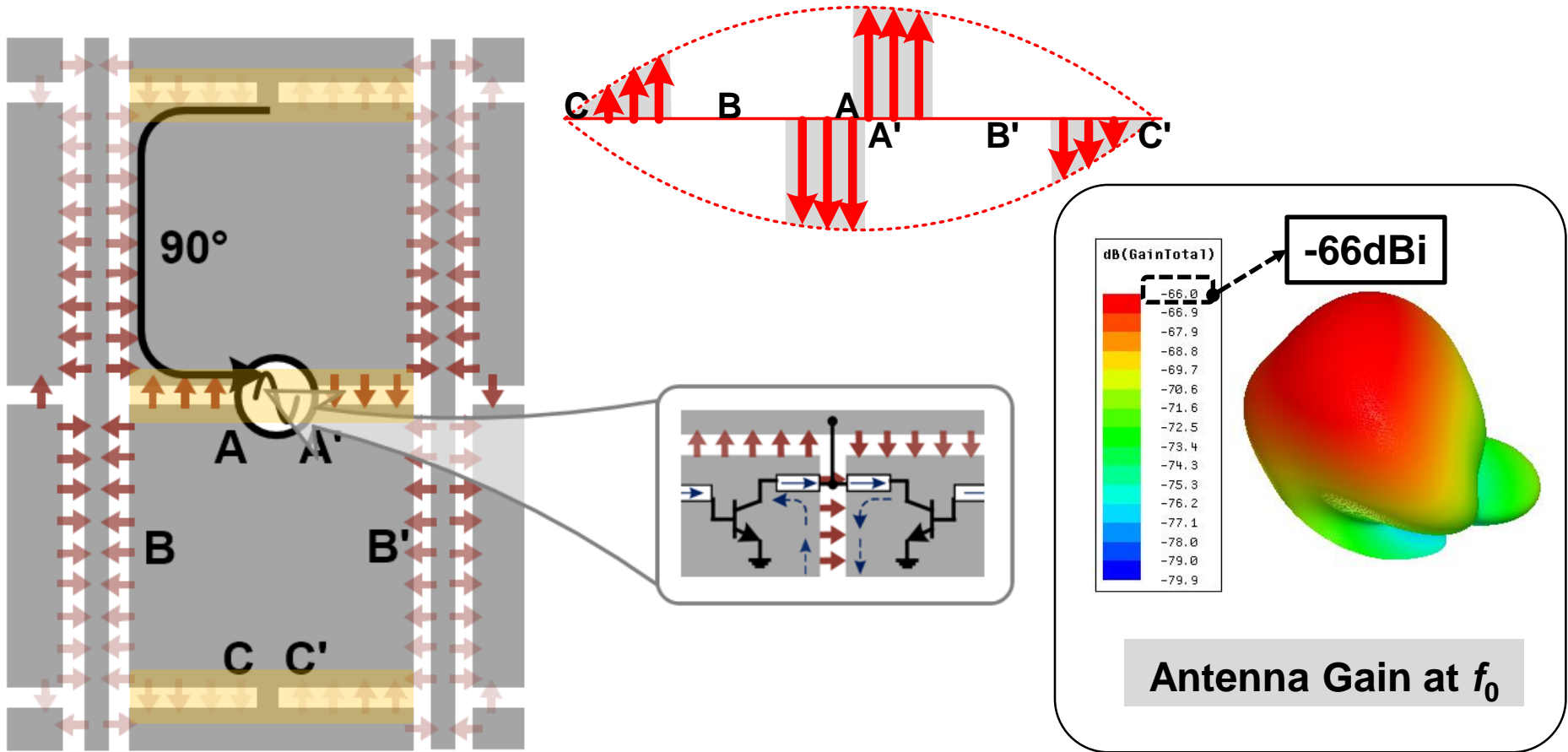


# Radiation Cancellation at $f_0$ (250 GHz): Vertical



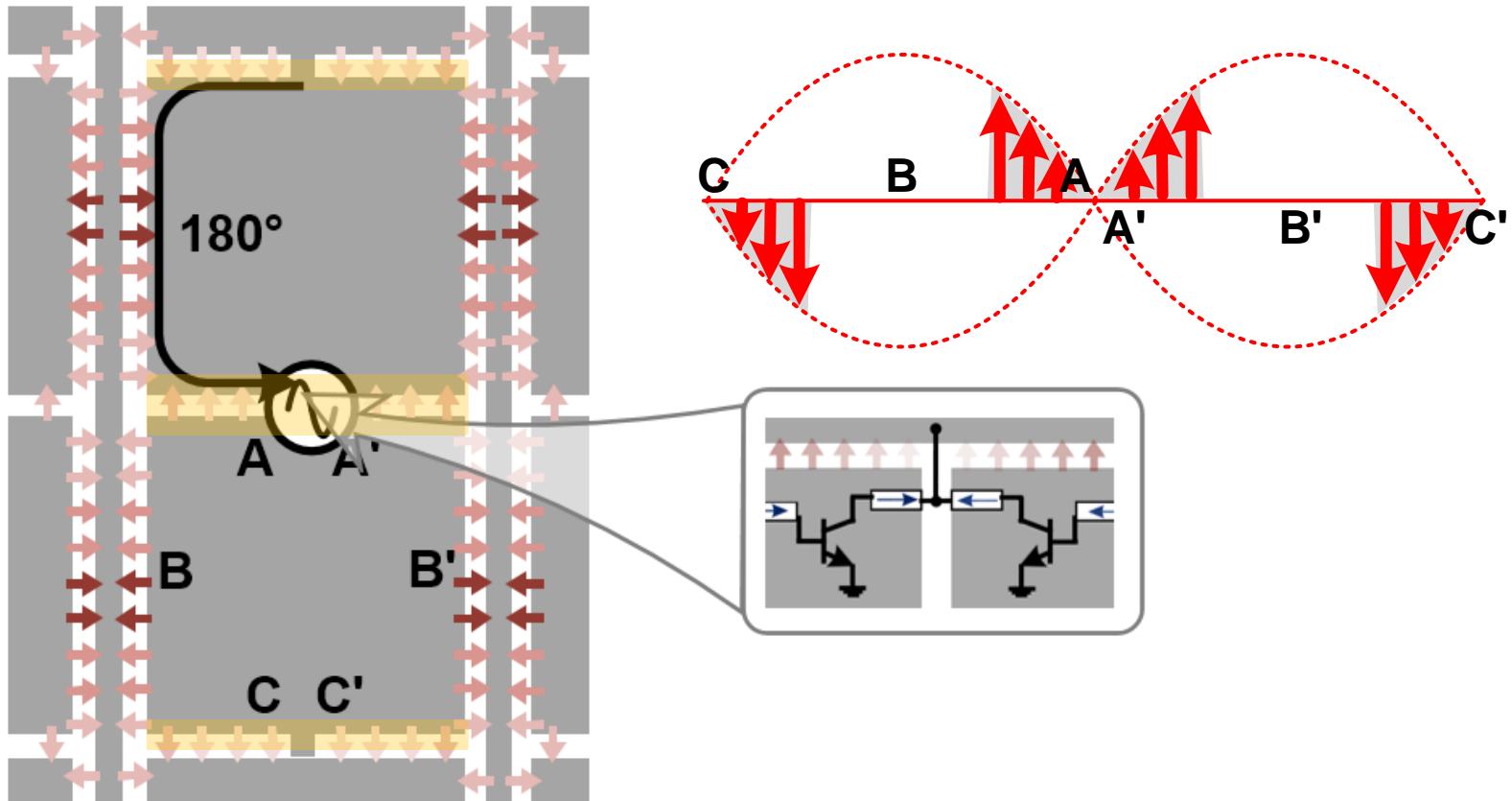
- **Vertical slotlines pairs do not radiate**
  - E-field in left and right slotlines balance out

# Radiation Cancellation at $f_0$ (250 GHz): Horizontal



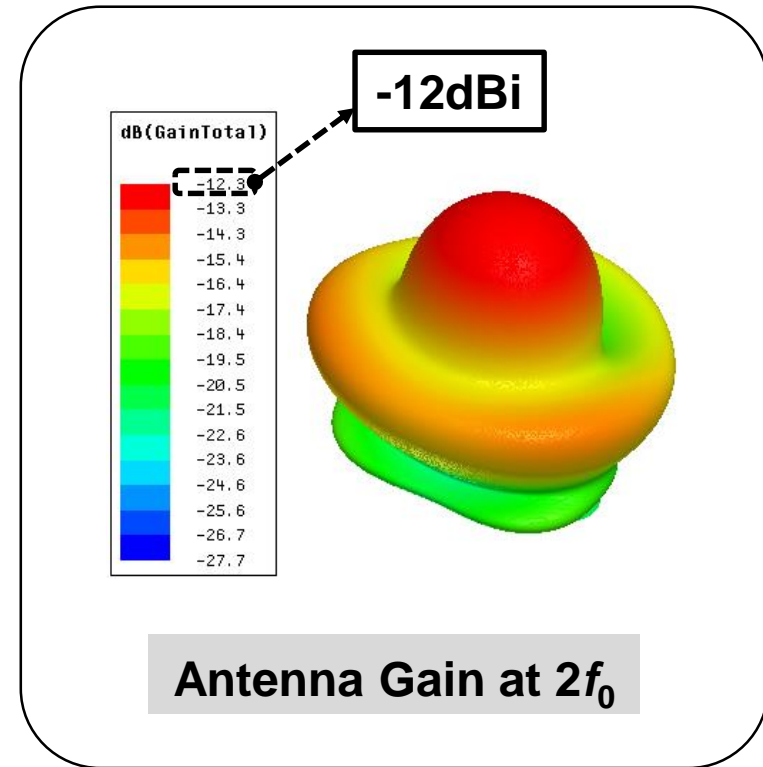
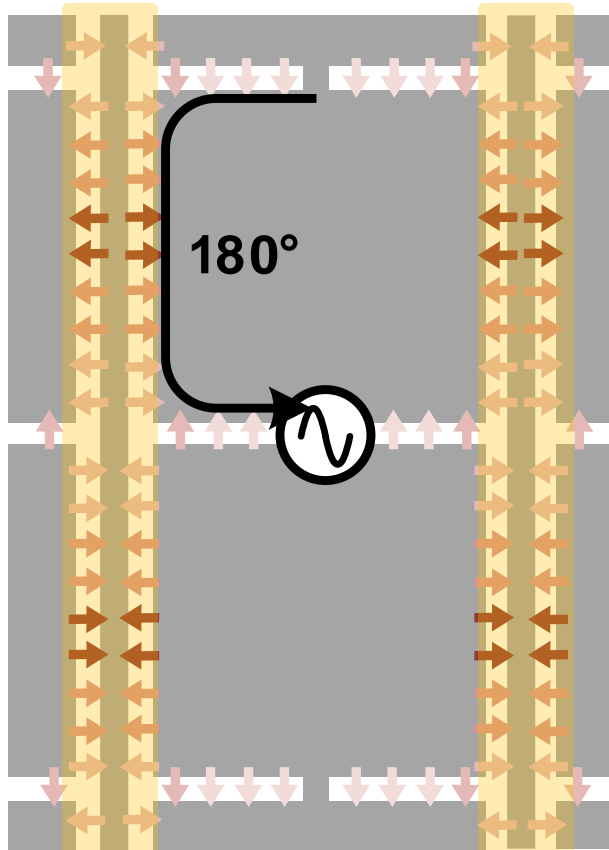
- **Horizontal slotlines pairs do not radiate**
  - E-field in left and right slotlines balance out

# Radiation Cancellation at $2f_0$ (500 GHz): Horizontal



- **Horizontal slotlines do not radiate**
  - E-field in central slotlines balance out with top/bottom slotlines

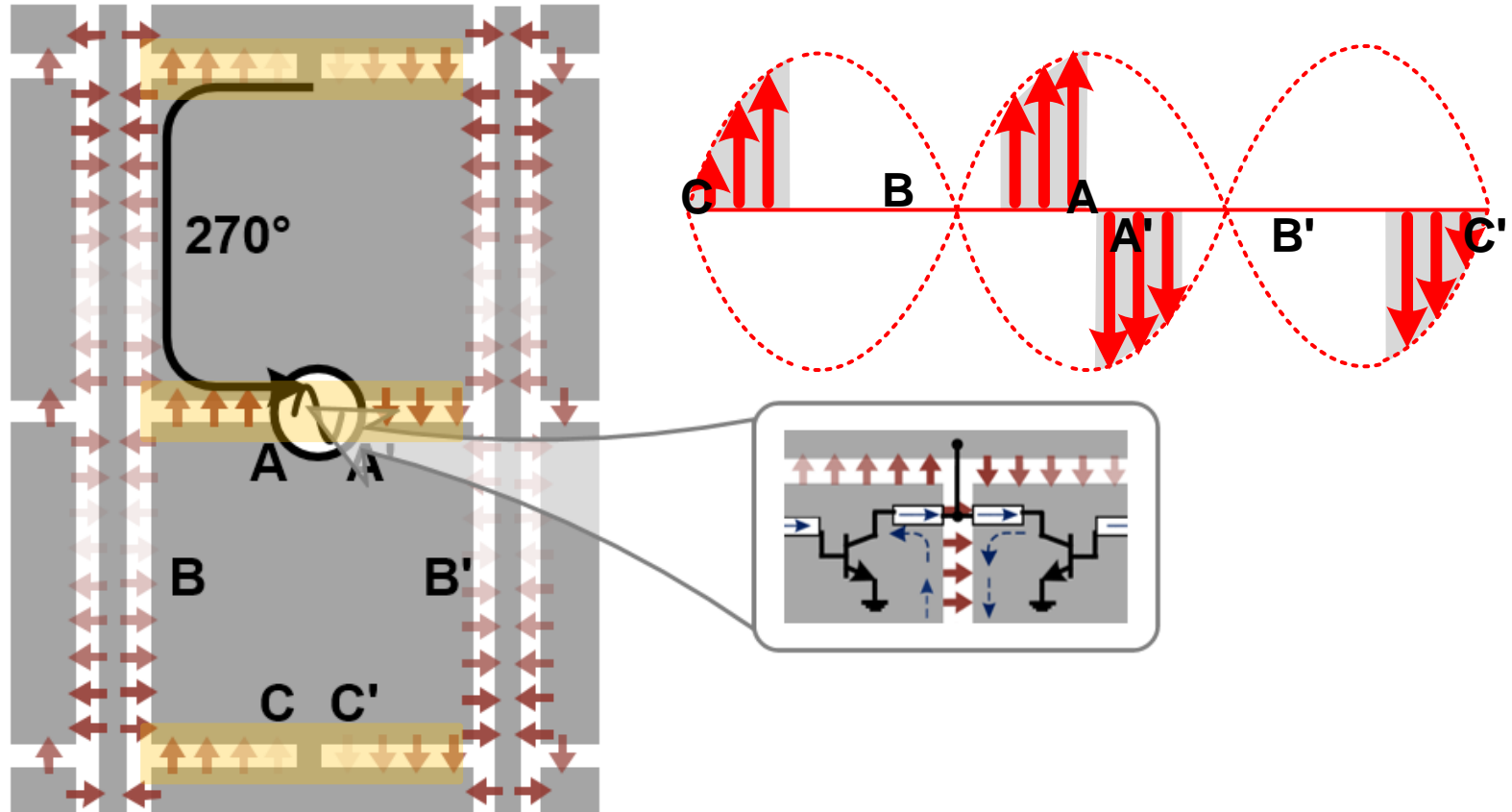
# Radiation Cancellation at $2f_0$ (500 GHz): Vertical



- **Vertical slotlines pairs do not radiate**
  - E-field in left and right slotlines balance out

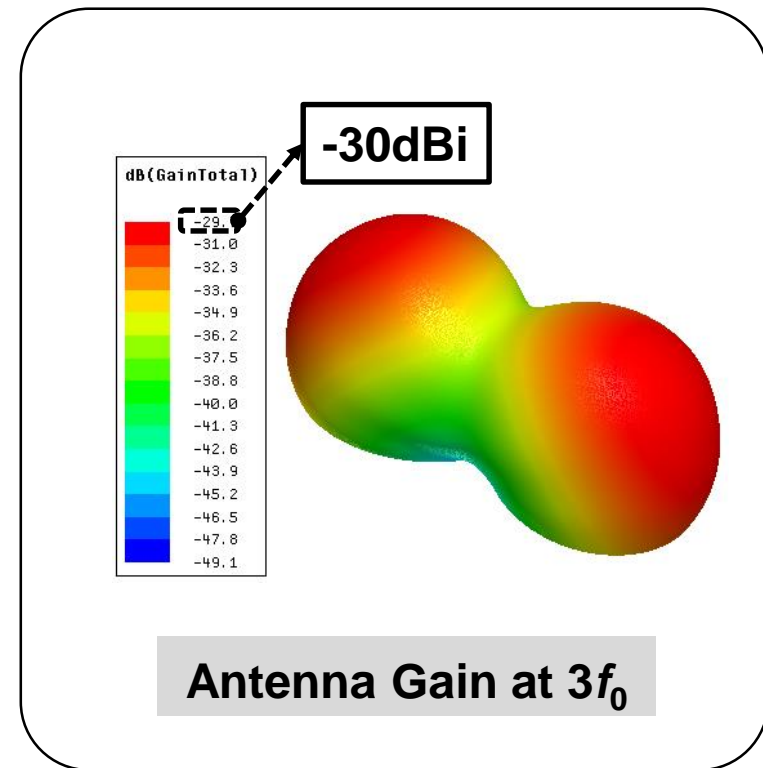
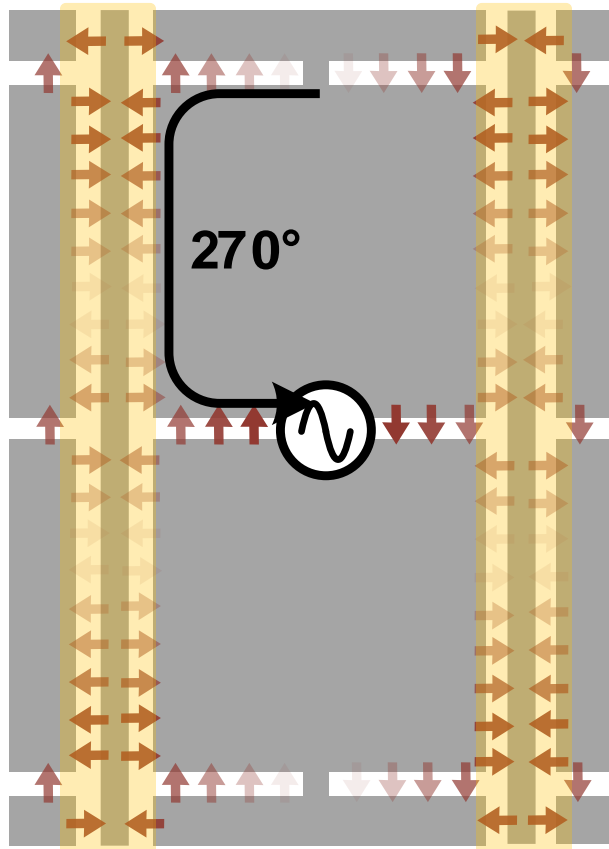


## Radiation Cancellation at $3f_0$ (750 GHz)



- **Horizontal slotlines pairs do not radiate**
  - E-field in left and right slotlines balance out

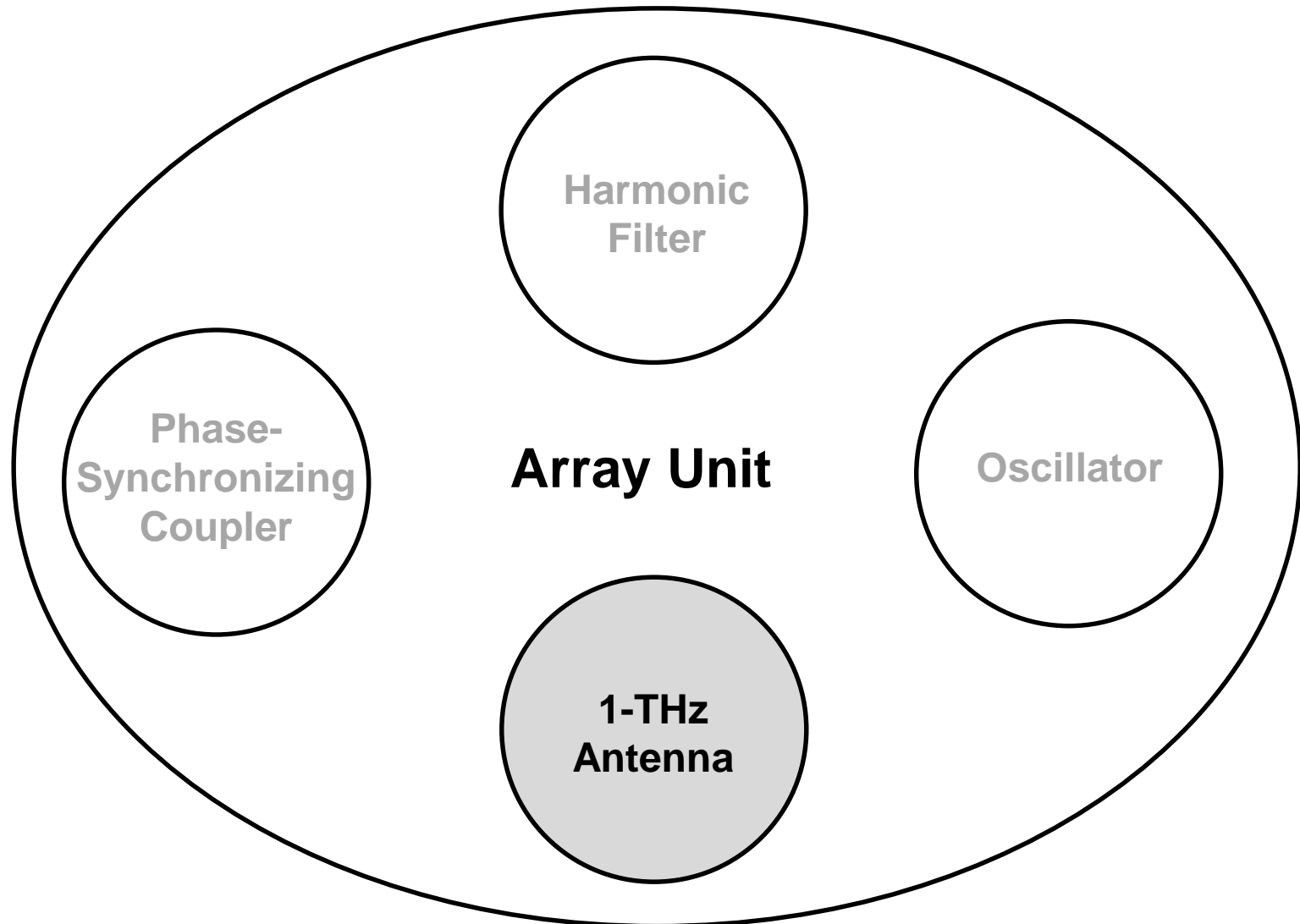
# Radiation Cancellation at $3f_0$ (750 GHz)

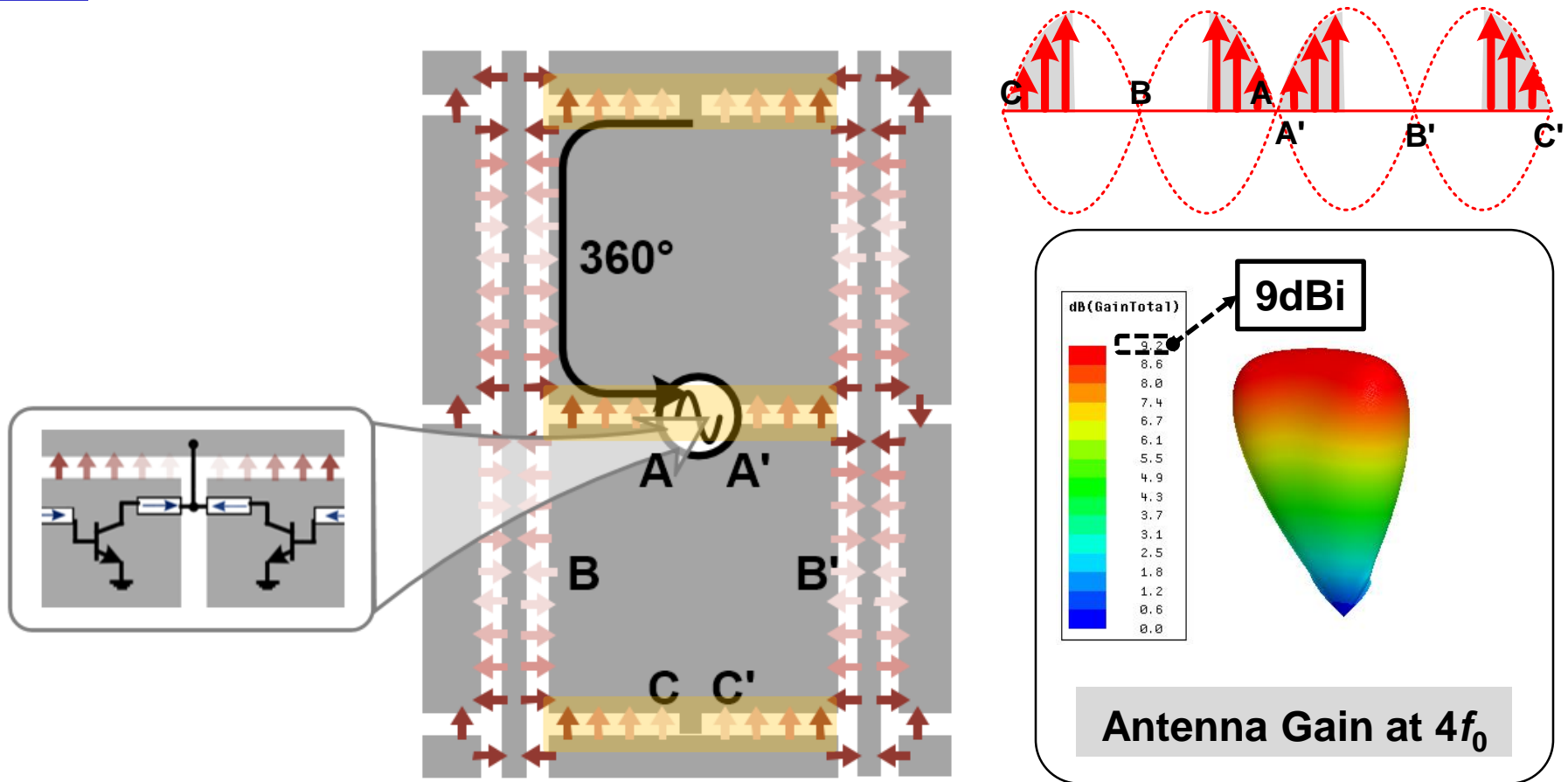


- **Vertical slotlines pairs do not radiate**
  - E-field in left and right slotlines balance out



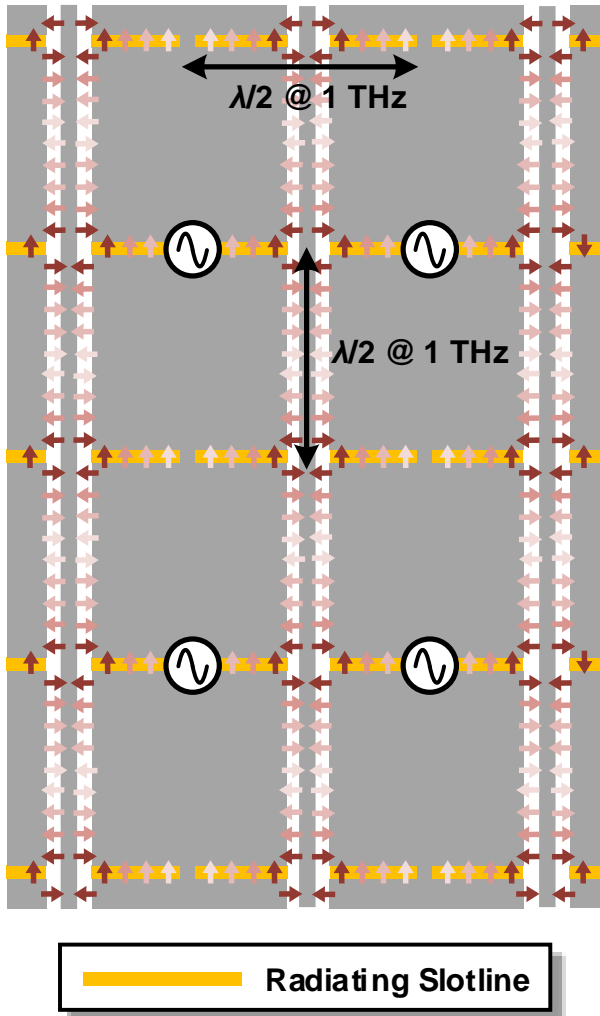
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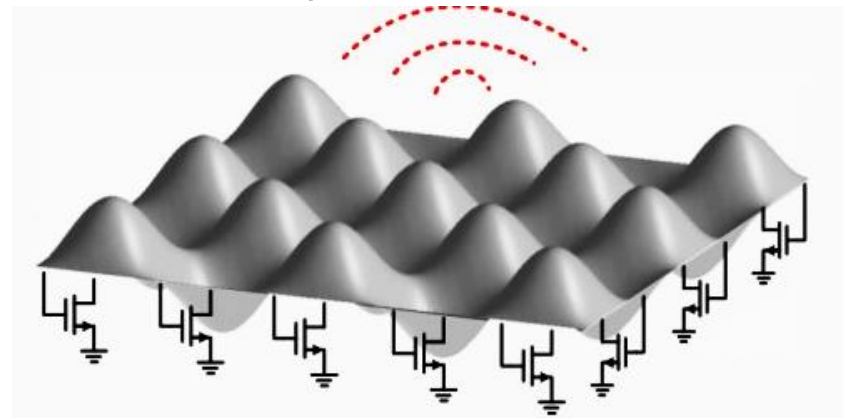
Radiation at  $4f_0$  (1 THz) from Single Unit

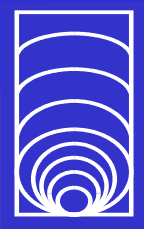
- All horizontal slotlines pairs radiate in-phase
- Vertical slotlines do not radiate

# 1-THz Radiating Array



- In-phase radiation from all units is achieved by CPW and slotline coupling
- 1-THz antennas are spaced by  $\lambda/2$  in both horizontal and vertical directions
- Equivalently, the array is like an “active planar wave front” with big aperture underpinned by transistors

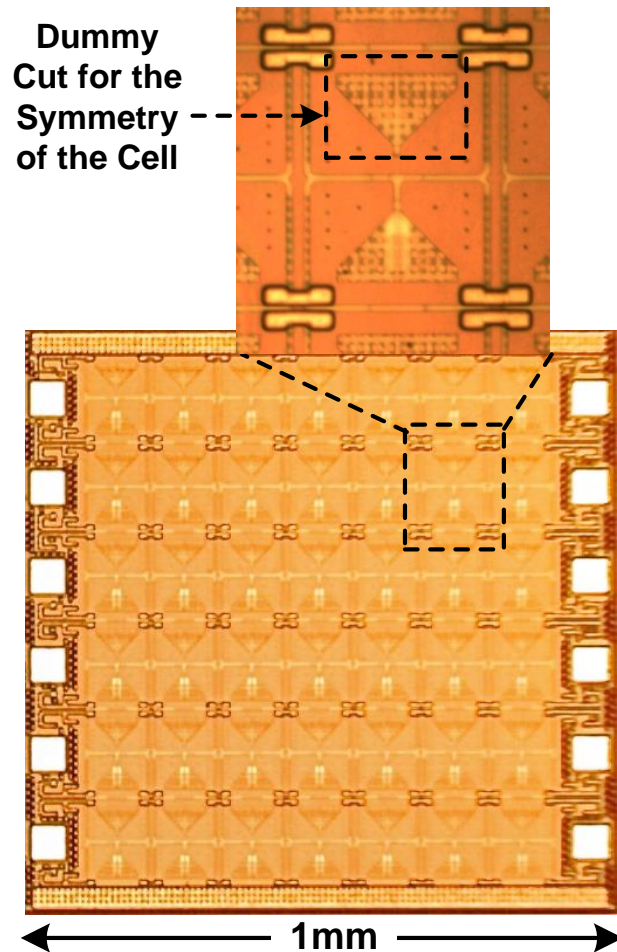




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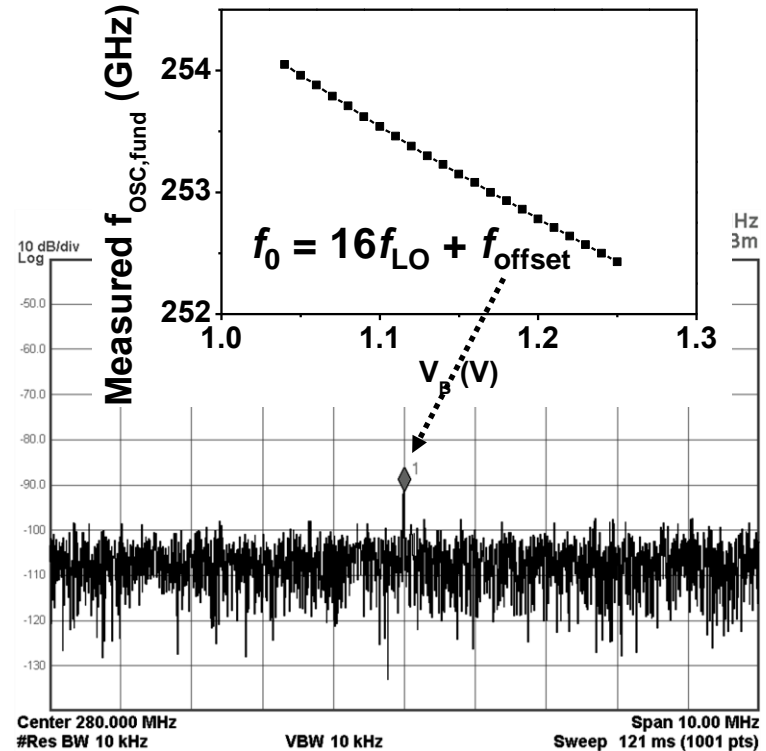
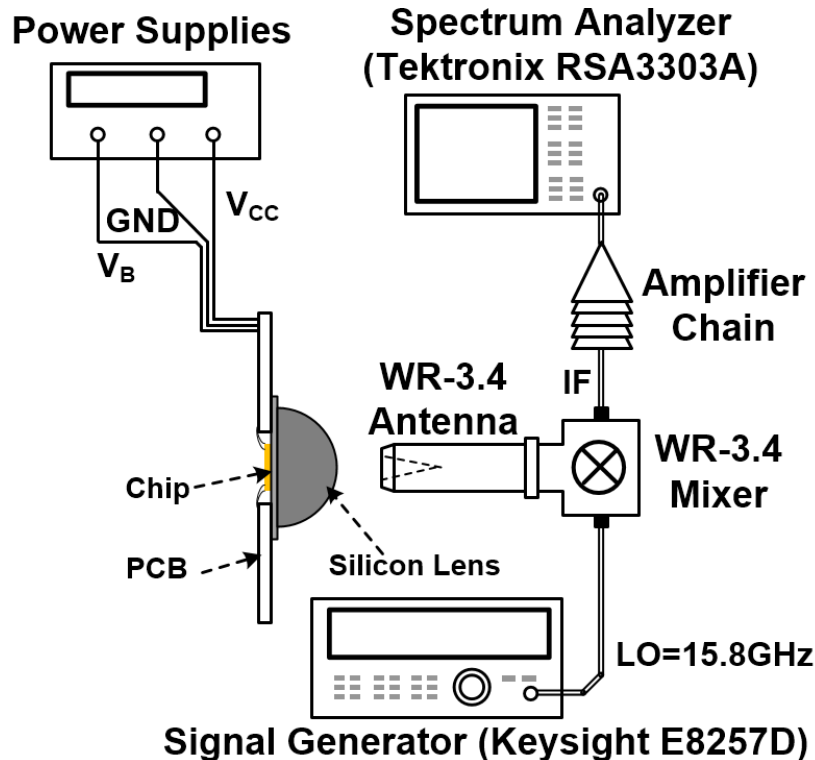
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## SiGe Chip Prototype



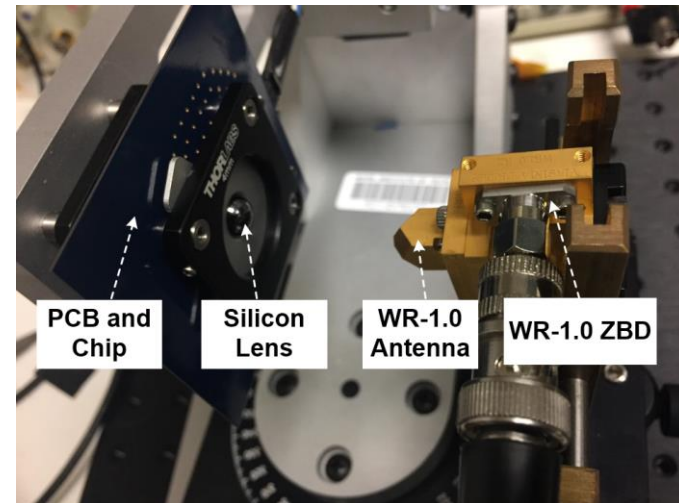
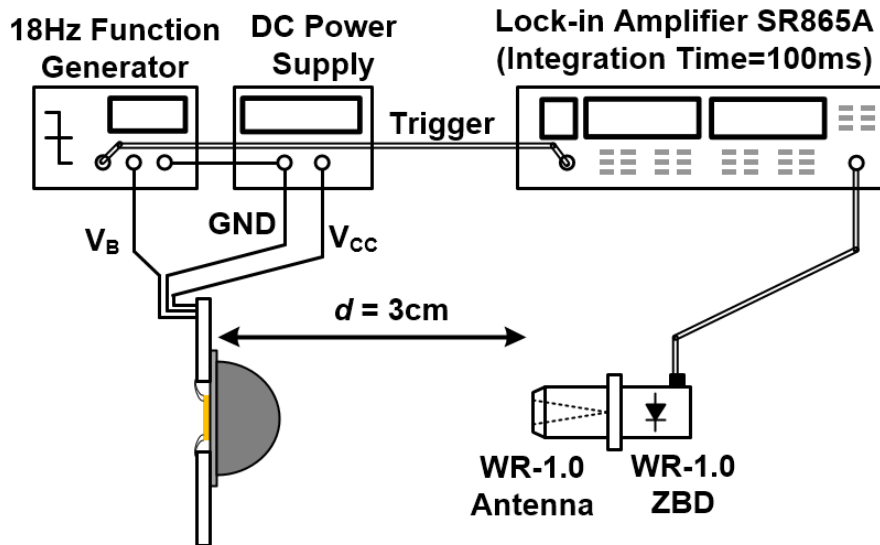
- **Technology: IHP S13G2 SiGe BiCMOS**
  - $f_{\max} = 450$  GHz
- **Area: 1 mm<sup>2</sup>**
- **Array scale**
  - 42 units
  - 91 antennas
- **DC Power: 1.1 W**

# Measurement of Spectrum of Leaked Fundamental



- Chip is attached to a half-ball silicon lens and radiates into backside
- Due to device mismatch, there will be little of  $f_0$  wave leaking out, with which we can confirm  $f_0$  and hence  $4f_0$

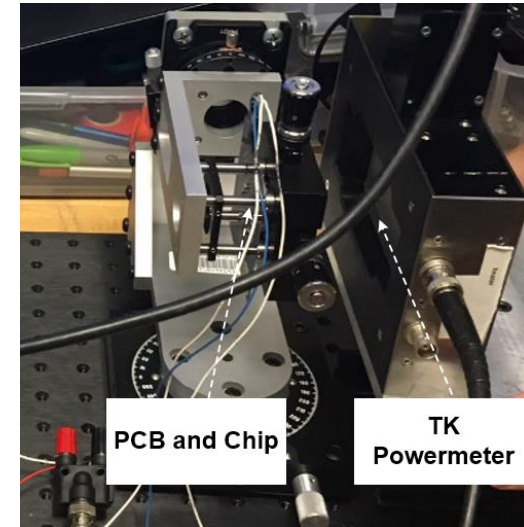
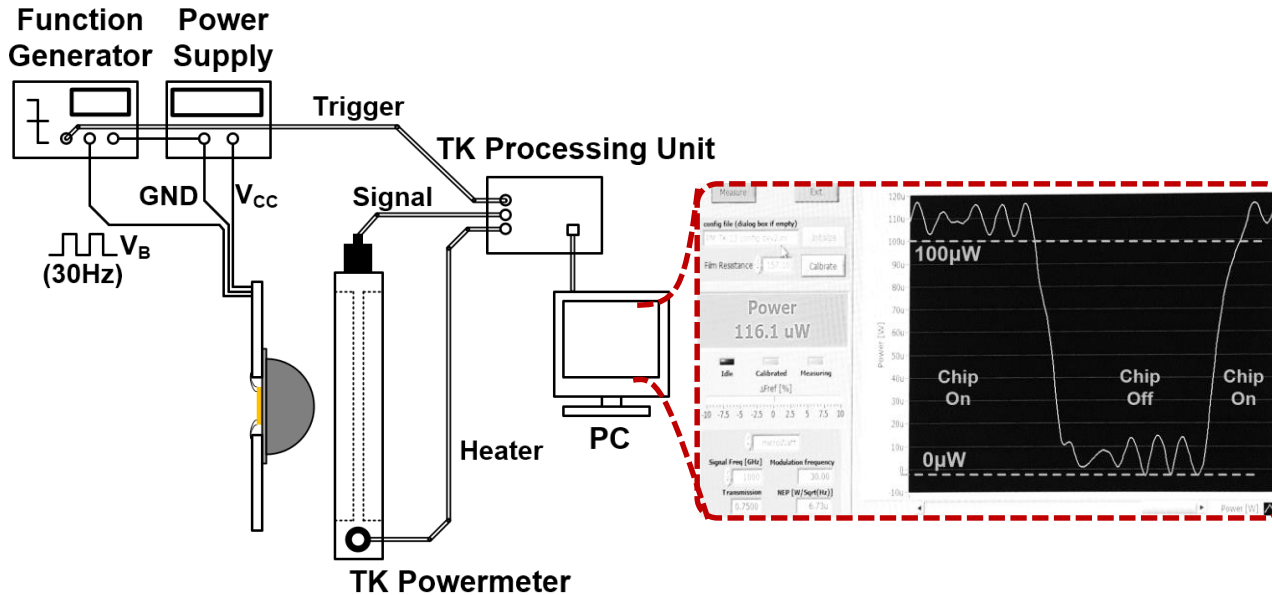
# Measurement of Total Radiated Power



## Measurement using VDI WR-1.0 zero-bias diode detector

- Total radiated power of 1 THz (from ZBD):  $80\mu\text{W}$  (-11dBm)

# Measurement of Total Radiated Power

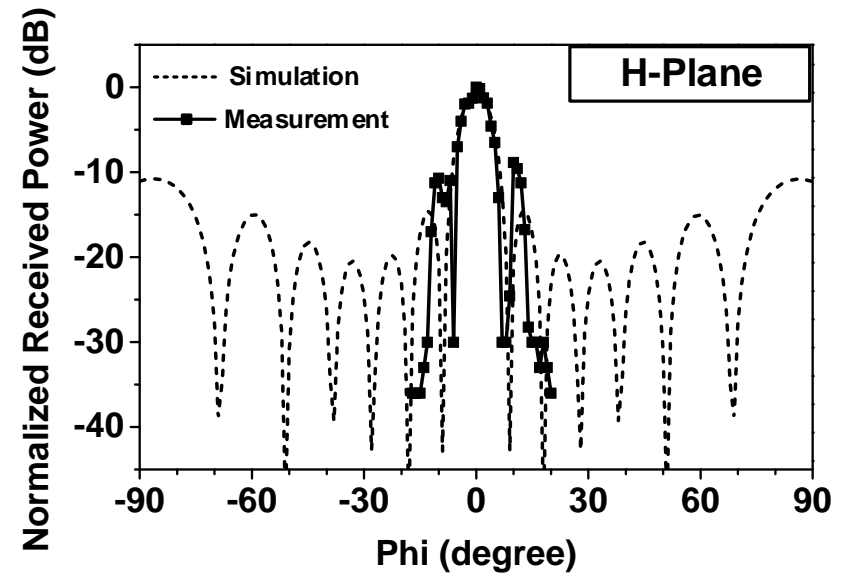
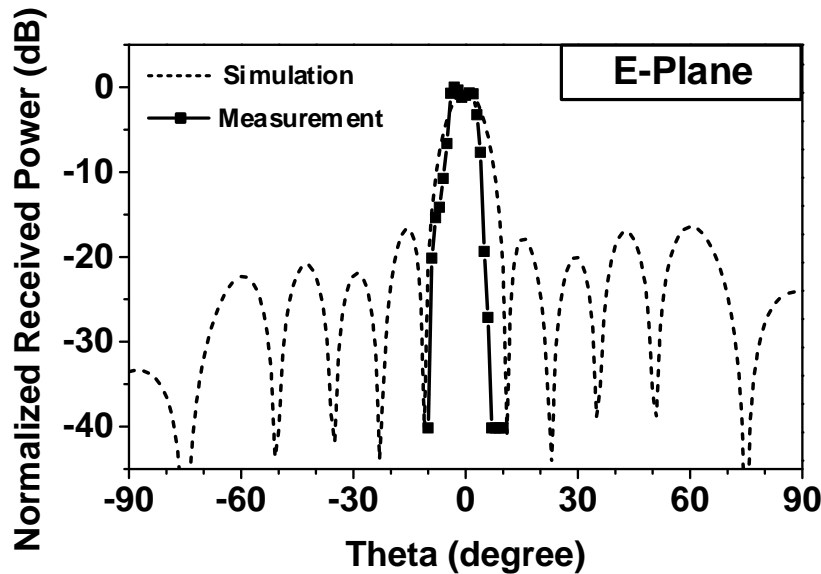


## Measurement using large-aperture Thomas Keating photo-acoustic powermeter

- Total radiated power of 1 THz (from ZBD): 80  $\mu$ W (-11dBm)
- Total radiated power of all harmonics (from TK): 100  $\mu$ W



# Measurement of Radiation Pattern



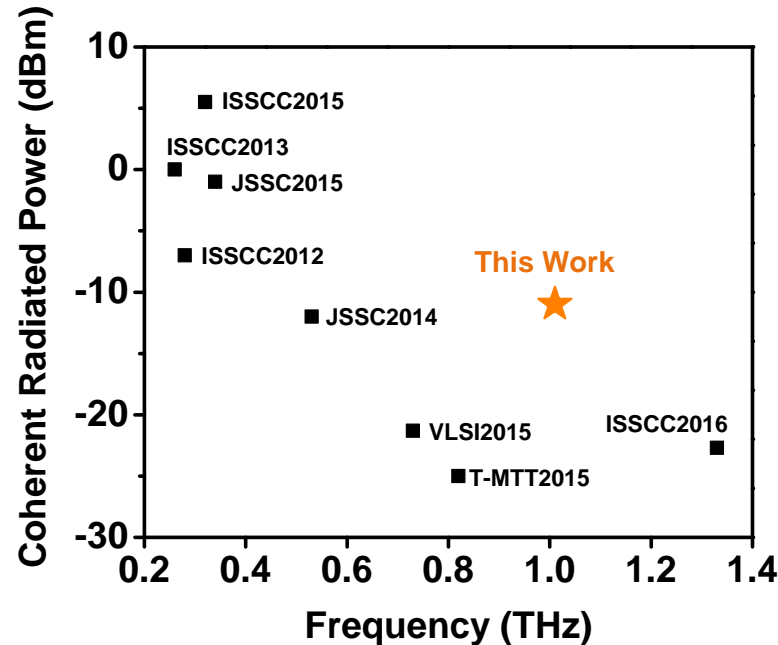
- Measured using zero-bias diode detector
- Peak directivity: 24dBi
- EIRP: 13dBm

## Performance Comparison

Reference	This Work	MTT2015	ISSCC2011	ISSCC2016	VLSI 2015
Circuit Type	Oscillator Array ( $4f_0$ )	Active Multiplier ( $6f_0$ )	Active Multiplier ( $5f_0$ )	Passive Multiplier ( $10f_0$ )	Passive Multiplier ( $5f_0$ )
Output Frequency (THz)	1.01	0.99	0.82	1.33	0.73
Radiated Power (dBm)	-10.9	N/A	N/A	-22.7	-21.3
EIRP (dBm)	13.1	-37	-17	-13	-22.2
Input RF Power (dBm)	N/A	8	14	18	13.8
DC Power (W)	1.1	4	3.7	0	0
Chip Area (mm <sup>2</sup> )	1.00	3.28	3.22	0.36	0.26
Technology	0.13 $\mu$ m SiGe	0.25 $\mu$ m SiGe	0.25 $\mu$ m SiGe	65nm CMOS	65nm CMOS

- Highest total radiated power
- Highest EIRP

## Conclusions



- **A high-power 1-THz radiator featuring 2D-coupled array architecture**
  - Large array scale
  - Directive radiated beam
- **Compact multi-functional structure will be an important component in future THz circuits**



## Acknowledgements

- **Analog Devices Inc.**
- **MIT/MTL GaN Energy Initiative**
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- **Prof. Qing Hu at MIT for chip testing support**
- **Dr. Mehmet Kaynak at Leibniz-Institut für innovative Mikroelektronik (IHP) for chip fabrication support**



Student  
Paper  
Finalist

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